A High Performance Hybrid Spectrometer for the Single Crystal Spectroscopy at the Pulsed SNS

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Outline

Scientific case and design objectives for the proposed hybrid spectrometer for the SNS

General layout of the proposed spectrometer and its place in the SNS instrument suite

Comparison of different spectrometer concepts and evolution of our thinking

Preliminary analysis of the instrument performance

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Scientific case for a proposed instrument for the SNS

Neutron spectrometer for studies of the coherent low-energy states in single crystals.

- □ Coherent collective excitations in single crystals:
 - lattice dynamics (phonons)
 - spin dynamics (magnons, critical scattering)
- □ Structure and dynamics of partially ordered and glassy states
 - spin glasses
 - charge glasses
 - correlated amorphous phases
- Study of the microscopic physical properties of samples in a variety of extreme environments:
 - magnetic field
 - pressure
 - temperature
- Characterization of spin-dependent cross-sections by means of polarization analysis



What are the typical samples we want to study?

CuGeO₃ sample used by M. Arai group for detailed measurement of the excitation dispersion on MAPS in 2000



Benchmark requirements for a single crystal neutron spectrometer

- Transmission of both primary (monochromator) and secondary (analyzer) spectrometers should be close to 1 within the resolution acceptance range, and vary smoothly over a substantial energy interval, typically from 2.5 meV to 60 meV.
- Both spectral (energy resolution) and angular (~ wavevector resolution) acceptances of the monochromator and analyzer should be flexible and easily adjustable, typical resolutions are 1% to 5%.
- Scattering volume seen by a detector should be well defined and easily adjustable depending on the sample size to minimize the background.
- Efficient use of the large incident neutron beam by focusing it on the sample is very important, and should be previewed.





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How does the instrument we propose fit SNS inelastic instruments suite?

High energy transfer

10-1000 meV Fermi Chopper Spectrometer

• E = 10 - 1000 meV

High intensity at moderate resolution and medium energy transfer + polarized beam Crystal Monochromator Hybrid Spectrometer

• Q = 0.1 - 8 Å⁻¹



High resolution and low energy transfer

10-100 µeV Multichopper Spectrometer

- E = 2 20 meV
- Q = 0.1 4 Å⁻¹





Schematic layout of the proposed Rotating Crystal Time-of-Flight Spectrometer



How does the instrument we propose fit SNS floor layout?

Needs rather short, 15 to 25 m primary flight path, but large, ~7-8 m radius floor area for the moving analyser bank and the sample table.



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Evolution of our concept: from multi-chopper TOF to chopper-less hybrid spectrometer

We choose to optimize the instrument performance at $E_i = 14.7 \text{ meV}$



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Pro's and Con's of a Fermi Chopper

- Advantages of a Fermi chopper
 - short burst times can be achieved with wide beams
 - works for very energetic neutrons
 - beam height is not limited
- Disadvantages of a Fermi chopper
 - is a rotating collimator with curved slots: limits the beam horizontal divergence, does not take full advantage of the guide
 - short burst times require tight collimation, i.e. reduced transmission and angular acceptance
 - is optimized for a fixed set of incident energies, changing energy or resolution requires changing the rotor
 - finite transmission away from the nominal angular position (especially at 180°) may lead to background and non-trivial beam contamination

does not focus neutron beam on the sample



Pro's and Con's of a Disk Chopper



- rotation rate is not correlated with neutron energy, resolution can be semi-continuously varied
- energy can be changed without impacting on transmission
- Disadvantages of a disc chopper
 - small burst width cannot be achieved with wide beams because tensile strength limits maximum rotation rate
 - transmission reduces when time for neutrons to traverse the disk becomes comparable with the slot open time (at lower neutron energies)
 - order contamination may occur when multiple slot discs are used
 - beam height is limited
 - does not focus neutron beam on the sample



Pro's and Con's of a Crystal Monochromator





What's Good About Rotating Crystal?

Defines the time structure of the neutron pulse at the sample: no chopper is necessary

Advantages of a rotating crystal monochromator short burst times can be achieved with wide beams without impacting on either transmission or collimation • burst time decrease with decreasing neutron wavelength • rotation rates are well below the tensile strength limit • takes full advantage of the horizontal divergence introduced by the supermirror-coated guide no impact on vertical focusing • possibility of time focusing (or defocusing) by changing the sense of rotation Disadvantages of a rotating crystal monochromator • introduces some Doppler broadening (but it decreases as the neutron wavelength increases) • ?



Technical case for the rotating crystal monochromator

A PG(002) crystal array 23 cm wide is needed to reflect a 4 cm wide beam of 60 meV neutrons

□ We assume a composite crystal monochromator, mounted on a 24 cm wide segmented vertically focusing device (GMI type), made of a high tensile strength AI alloy

□ At a rotation rate of 240 Hz the peripheral velocity of the frame is 181 m/sec, well below the maximum peripheral velocity (500 m/s) for high tensile strength Al alloys

□ At a rotation rate of 240 Hz the crystal velocity at the periphery of the spot illuminated by a 4 cm wide guide is about 5.1% of the velocity of a reflected neutron. For $E_i > 14.7$ meV this corresponds to a Doppler broadening of the incident energy distribution of less than 3.6%.

□ Narrowing the beam reduces the Doppler broadening, a phased disc chopper upstream could be used for Doppler focusing



Performance of the rotating crystal monochromator

- PG(002) rotating crystal viewing the m=3 supermirror guide
- Crystal mosaic 1.2°, downstream angular acceptance $\alpha_1 = 0.66^{\circ}$
- Secondary flight path 4.0 m

Crystal rotation rate (Hz)	Burst FWHM (µs	s) $\Delta t/t$	∆E/E
Ei=5.0 meV ($\alpha_0 = 2.4^\circ$)			
240	32	0.0065	1.3%
180	42	0.0105	2.1%
120	63	0.0158	3.2%
60	126	0.0315	6.3%
Ei=14.7 meV ($\alpha_0 = 1.4^\circ$)			
240	26	0.0111	2.2%
180	34	0.0146	3.0%
120	52	0.0223	4.4%
60	103	0.0441	8.8%
$Ei=60.0 \text{ meV} (\alpha_0 = 0.69^\circ)$			
240	22	0.0190	3.8%
180	29	0.0251	5.2%
120	43	0.0372	7.4%
60	87	0.0753	15.6%



Secondary flight path and analyzer performance

Uncertainty of the flight time in the analyzer gives largest contribution to the energy resolution.



Choice of the moderator

"Benchmark" the instrument performance at $E_i = 15 \text{ meV}$



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Performance of the guide.

Impact of the guide curvature (relative to the similar straight guide) Impact of the guide coating (relative to $3\theta_c$ supermirror guide)



□ L = 20 m curved $3\theta_c$ supermirror guide at a reasonable offset of 8 cm ~ 2 times the width of the guide provides ~75% transmission at 60 meV □ Shorter (L = 15 m?) but narrower (3 cm?) guide may still be O.K.



Punchline: technical features of a proposed direct geometry hybrid instrument for the SNS

Efficient vertical focusing provides reasonable data collection rates even for very small samples !



