



# ***Superconductor status and prospects***

Peter J. Lee (Presenter)

with lots of help from Ron Scanlan (LBNL), Rob Hentges et al. (OI-ST), Eric Gregory (IGC-AS), Bruce Zeitlin (Supergenics), Arup Ghosh (BNL), Takao Takeuchi (NRIM)

David C. Larbalestier, Christopher D. Hawes, Michael T. Naus and Alexander A. Squitieri (UW-Madison)



**Very Large Hadron Collider**

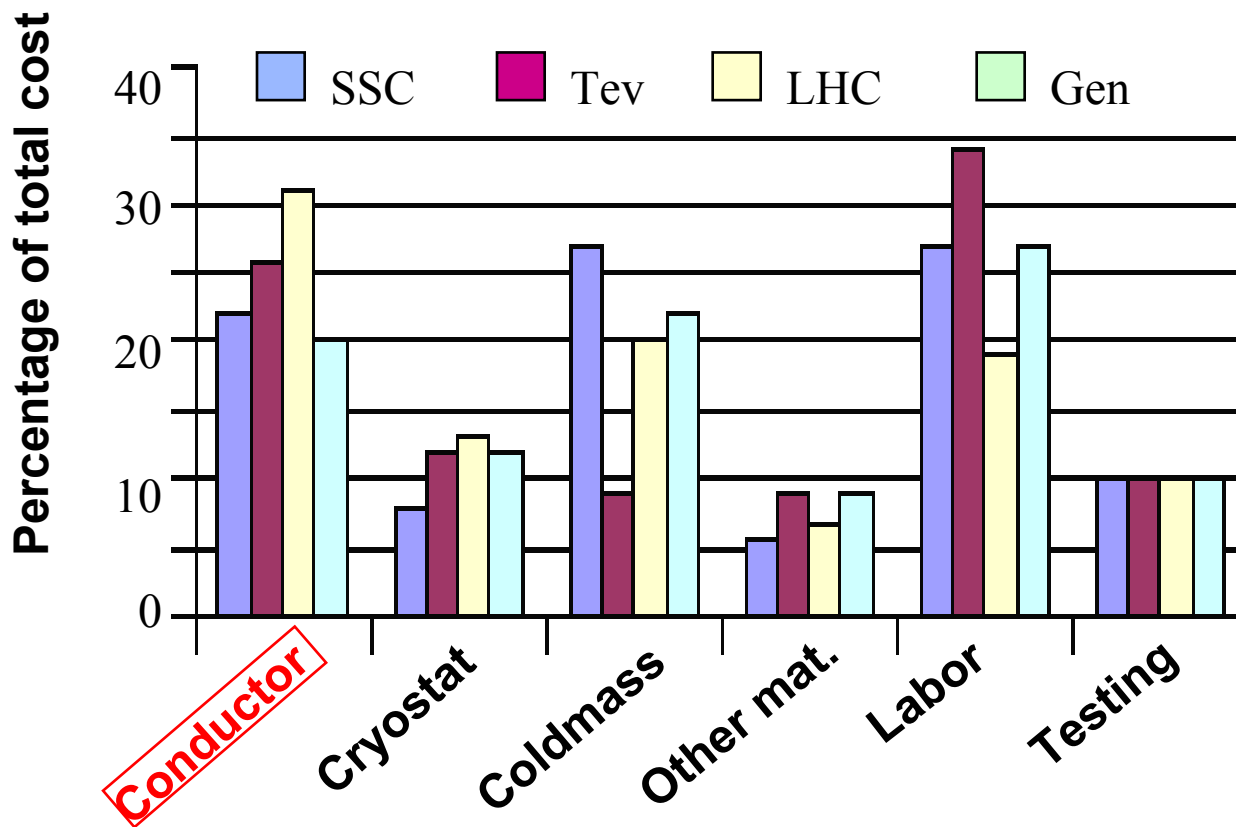
UW Work  
Sponsored by:





# Where to save \$?

## Start with the conductor



Steve Gourlay  
chart via  
Ron Scanlan  
ASC2000



$$C_{\text{dipole}}(\$) = 3.2\pi B\rho 2560 \left( \frac{r+0.5}{2} \right)^{0.43} (0.25 + 0.55(8/L_d)^{0.6}) (0.3 + 0.7(B/4.3))$$

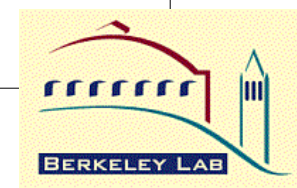
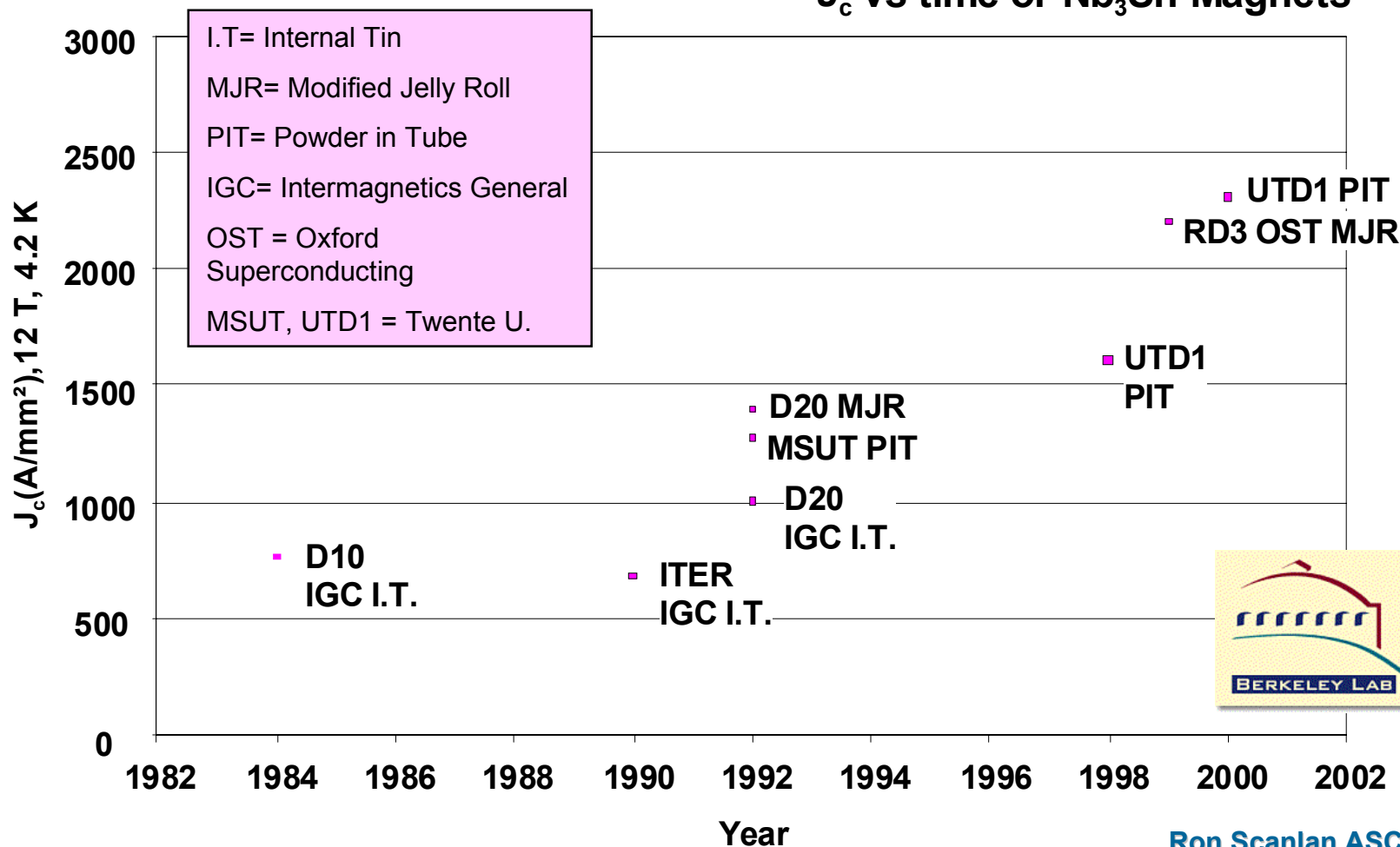
RHIC scaling





# Improvements in $J_c$ for $Nb_3Sn$

$J_c$  vs time or  $Nb_3Sn$  Magnets

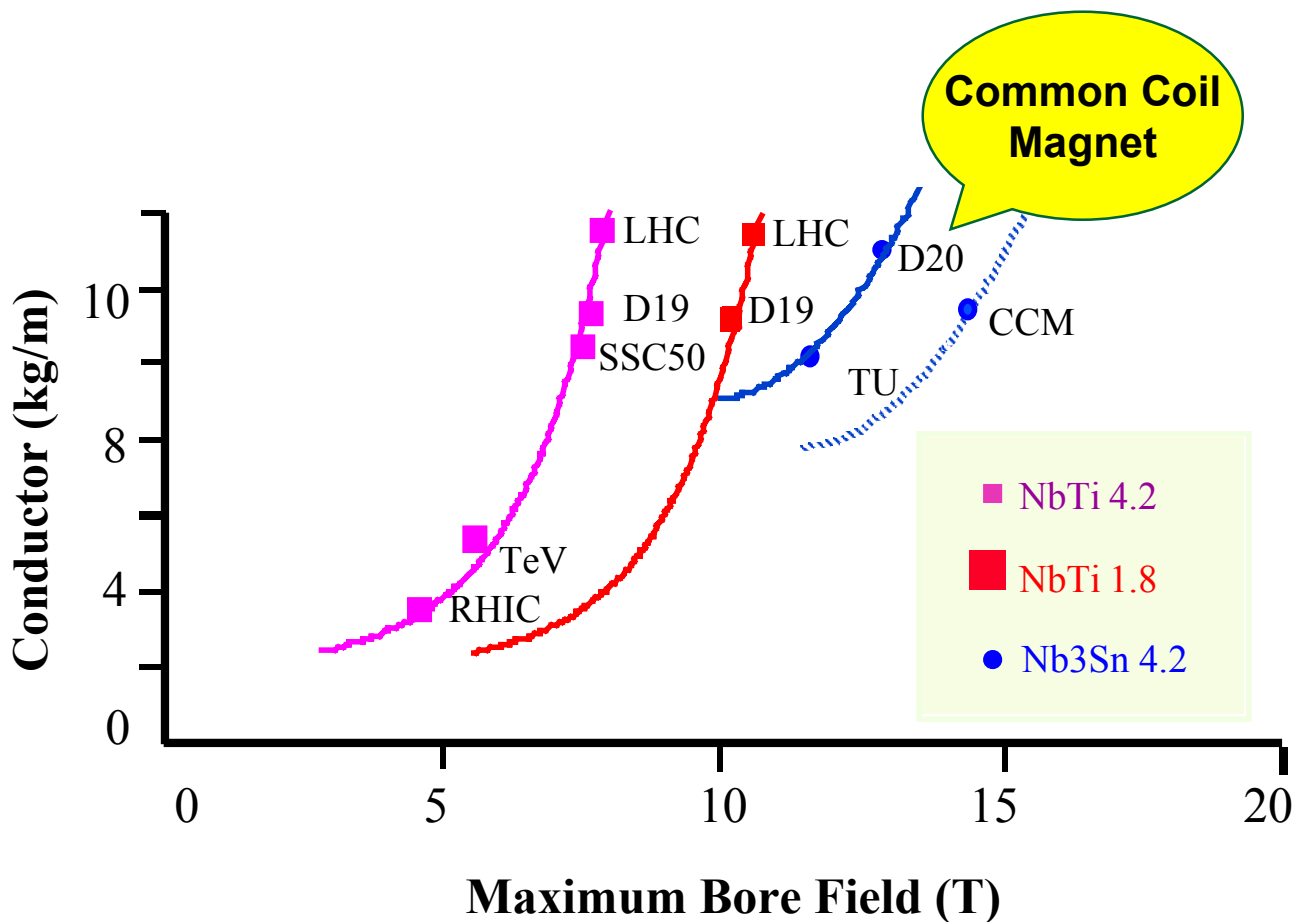


Ron Scanlan ASC2000





# Better materials & simpler coil geometry reduce conductor use



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***Major Development This Year:  
We now have a conductor  
development program that can fund  
industrial R&D outside SBIR box***

- Funded programs at OI and IGC
- Improved Interaction with manufacturers
- Conductor progress in most areas





# CDP Goals

- Provide a cost-effective, high-performance superconductor of qualities not yet achieved for the high-field magnets required for the next generation high-energy physics colliders
- Target specifications for the HEP conductor include:

$J_c$  (non-Cu, 12 T, 4.2 K):

3000 A/mm<sup>2</sup>

Effective filament size:

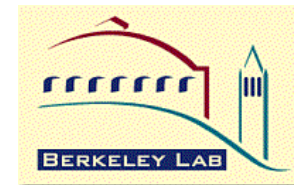
40  $\mu$ m or less

Piece length:

Greater than 10,000 m in  
wire diam. of 0.3-1.0 mm

Wire cost:

Less than \$1.50/kA-m (12 T, 4.2 K)

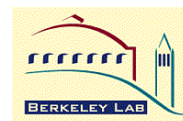
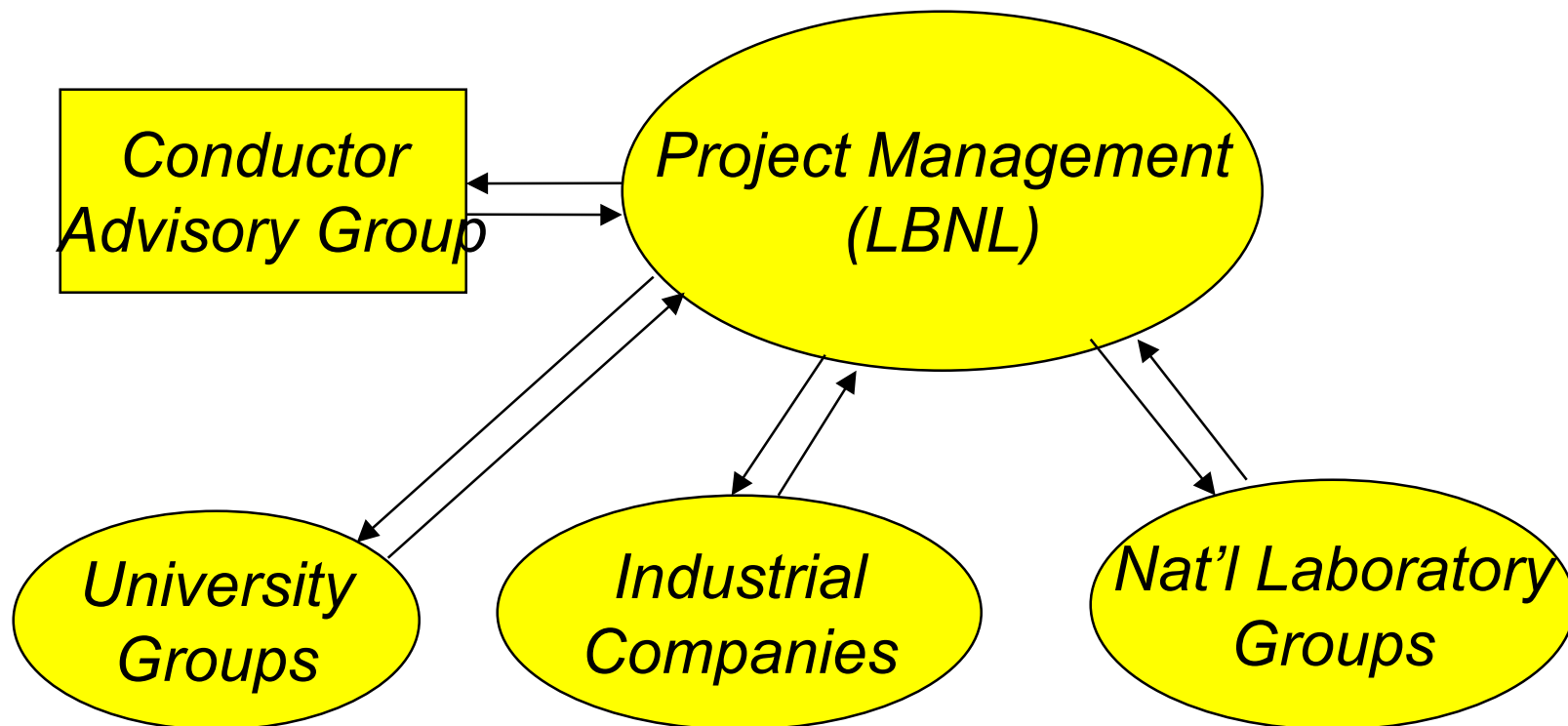


From:  
Ron Scanlan ASC2000





# Conductor Development Program Organization



Ron Scanlan ASC2000





# *The CD Group provides*

- Input to program plans and goals
- Technical support for the manufacturing R&D work
- Member organizations are BNL, FNAL, LBNL, OSU, TAMU, and U.Wisconsin-Madison
  - A. Ghosh(BNL)
  - P. Wanderer(BNL)
  - G. Ambrosio(FNAL)
  - P. Limon(FNAL)
  - D. Dietderich (LBNL)
  - R. Scanlan(LBNL)
  - E. Collings(OSU)
  - P. McIntyre(TAMU)
  - P. Lee(U.Wisc.)
  - D, Larbalestier(U.Wisc)
  - B. Strauss(DOE)
- Other contributors include: conductor R&D teams at IGC(see ASC 2000 paper 4MK07) and OST(see ASC 2000 paper 4MK08)



Ron Scanlan ASC2000







# ***Lab and University Support for FY00 is coming from base program funds***

- BNL(Suenaga): Heat Treatment (HT)
- FNAL(Barzi): HT,  $I_c$  tests
- LBNL(Dietderich, Higley): HT, characterization, cable development
- OSU(Collings, Sumption): Magnetization measurements
- TAMU(McIntyre, students): HT
- U. Wisc(Lee, students): HT, characterization,  $I_c$  tests

Total new funding for FY00:

\$500K	direct DOE	( IGC+OST contracts)
\$1,500K	DOE SBIR	support for Nb <sub>3</sub> Sn
\$1,100K	DOE SBIR	support for Nb <sub>3</sub> Al

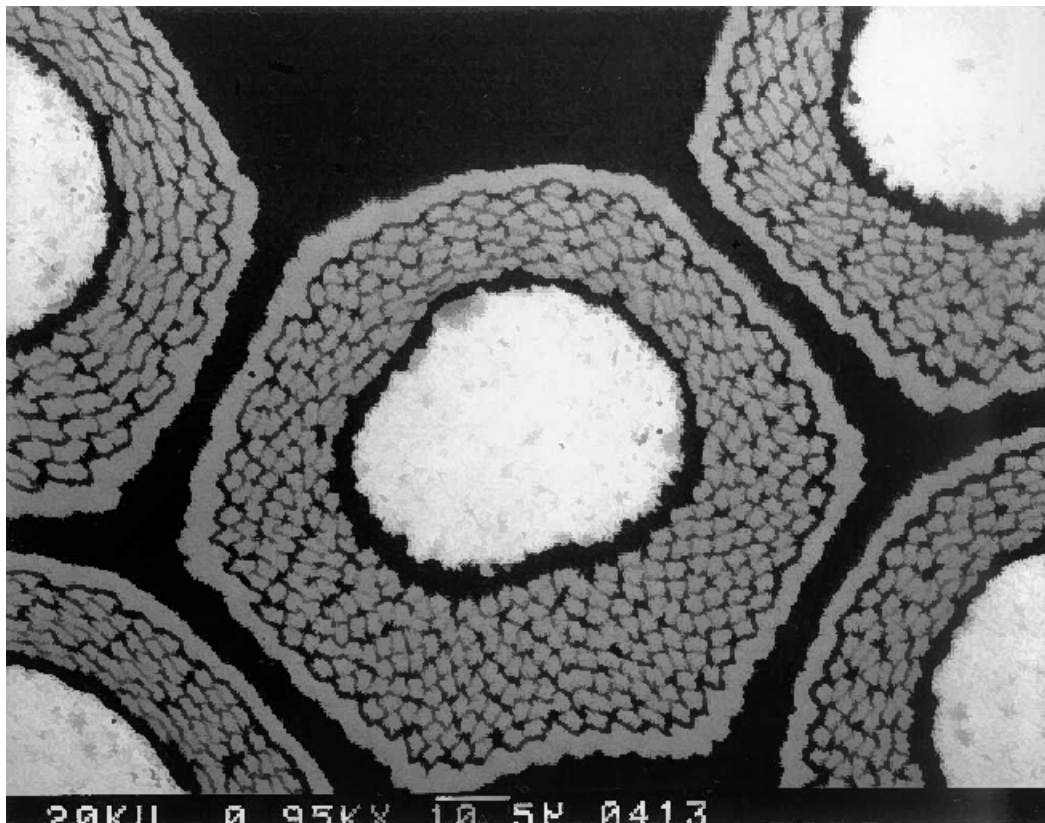


**Ron Scanlan ASC2000**



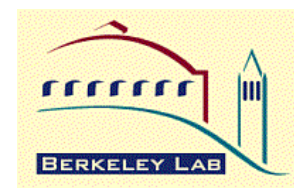


# MJR Conductor used in LBNL Magnet RD-3



- $J_c > 2000 \text{ A/mm}^2$   
(12 T, 4.2 K)
- $D_{eff} = 70 \mu\text{m}$
- $RRR = 3-15$

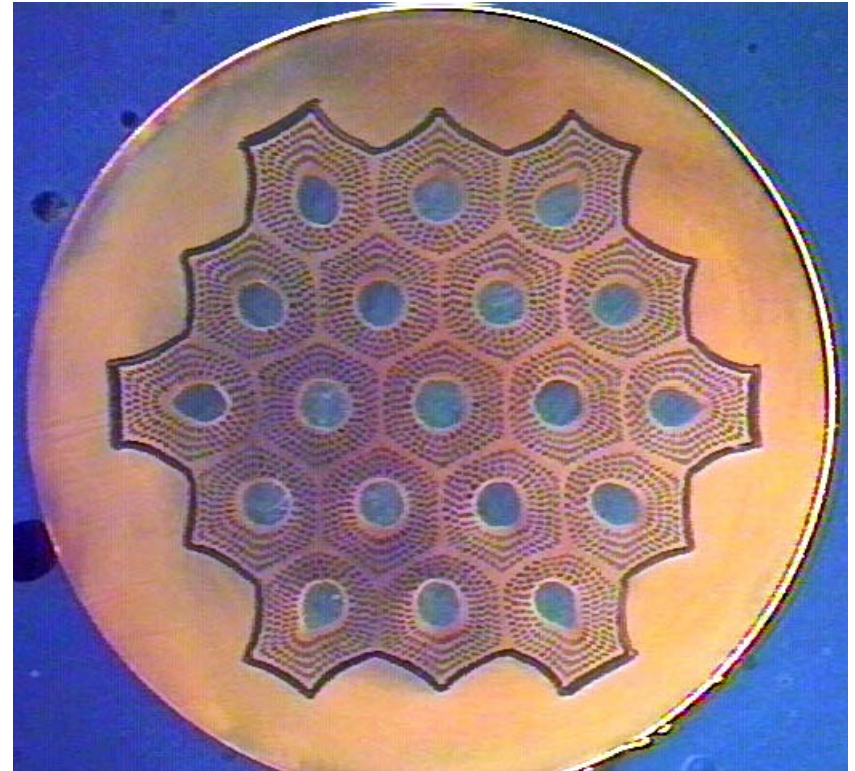
Ron Scanlan ASC2000





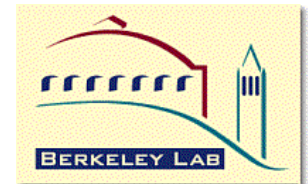
# OI-ST Goals

- Develop the Hot Extruded Rod (HER) process as a new, cost-effective alternative to their MJR process
- Determine  $J_c$  vs filament size relationship for HER process
- Optimize composition to give maximum  $J_c$



*HER process billet after extrusion, before salt is removed from cores*

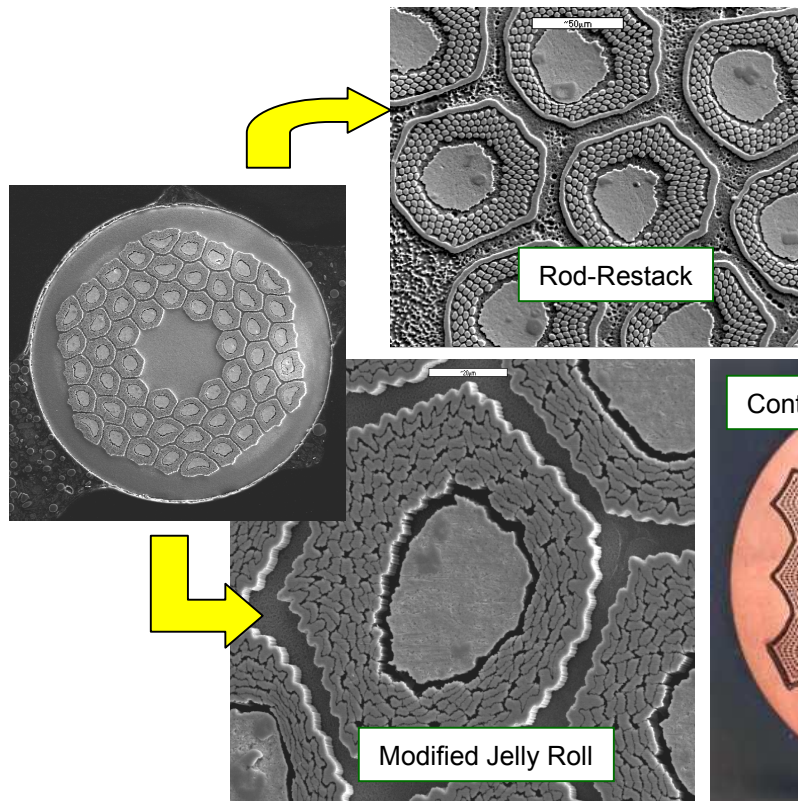
Ron Scanlan ASC2000





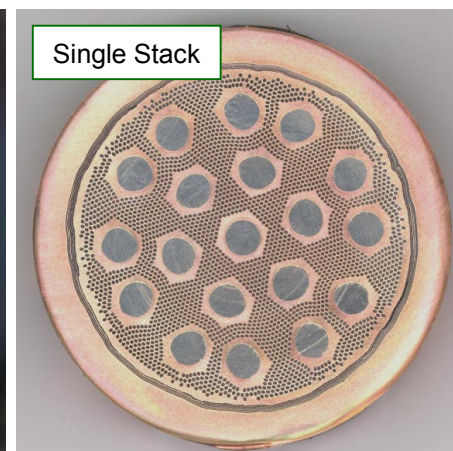
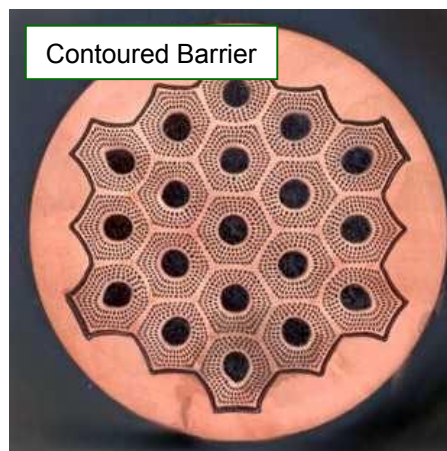
# OI-ST Internal Sn designs seeking lower cost and higher performance

Internal Tin



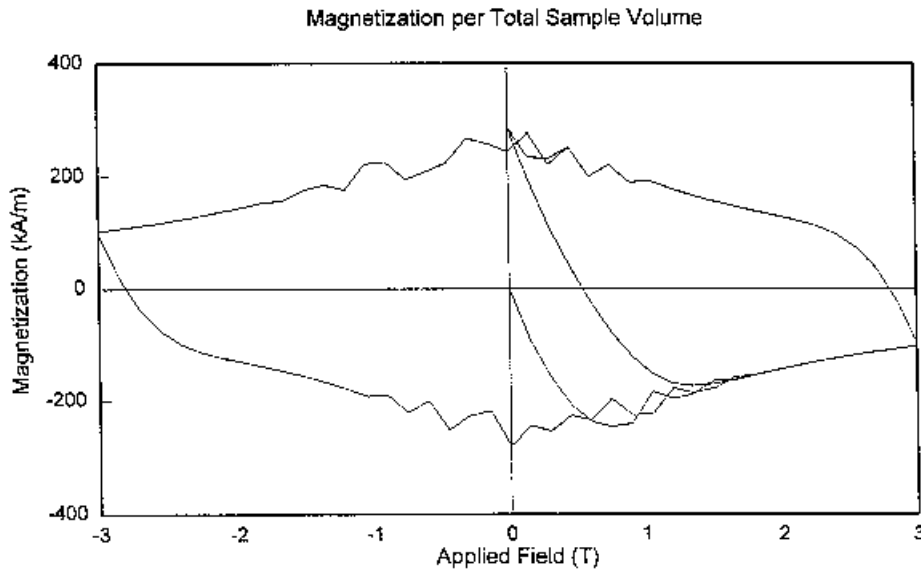
Hentges et al. (OI-ST) ASC 2000

OXFORD



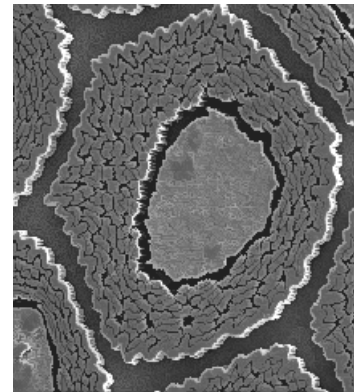


# Magnetization of MJR



- Minor flux jumps  $< 2$  T
- $D_{\text{eff}} \sim 80\text{-}100 \mu\text{m}$
- $D_{\text{eff}}$  approximates diameter of filament bundle

Data from NIST



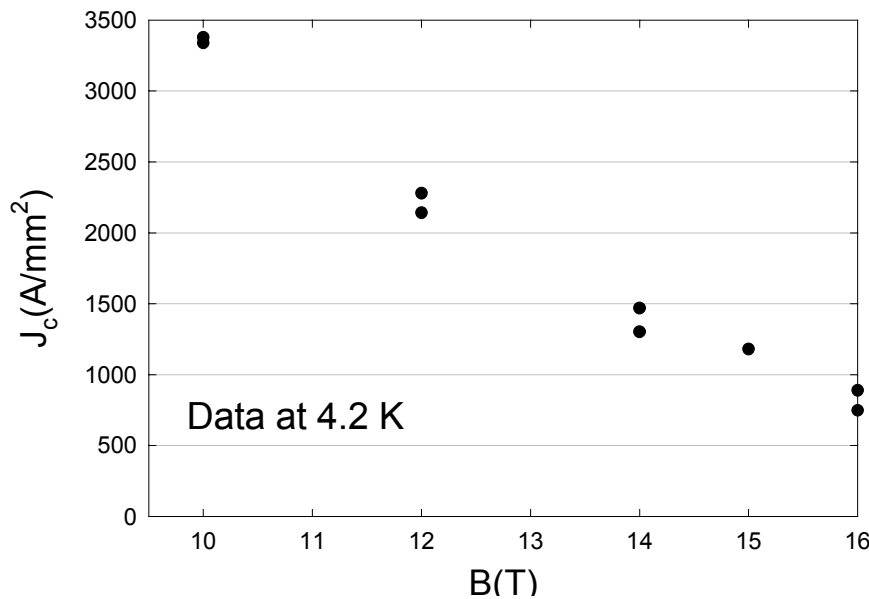
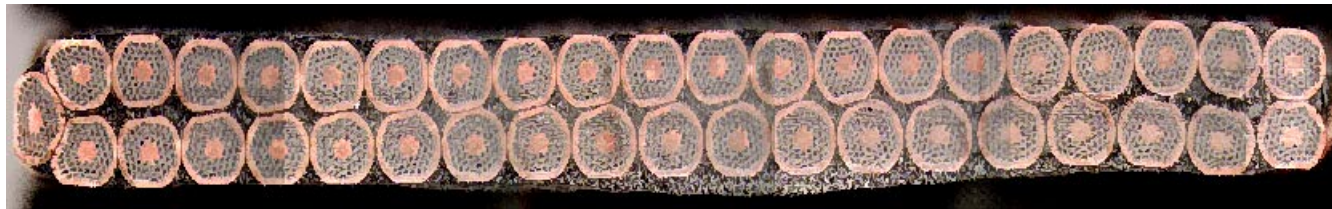
OXFORD

Hentges et al. (OI-ST), ASC 2000





# LBNL MJR Cable Results



- 10 T  $J_c \sim 3200$  A/mm<sup>2</sup>
- 12 T  $J_c \sim 2100$  A/mm<sup>2</sup>
- 14 T  $J_c \sim 1300$  A/mm<sup>2</sup>
- 16 T  $J_c \sim 750$  A/mm<sup>2</sup>



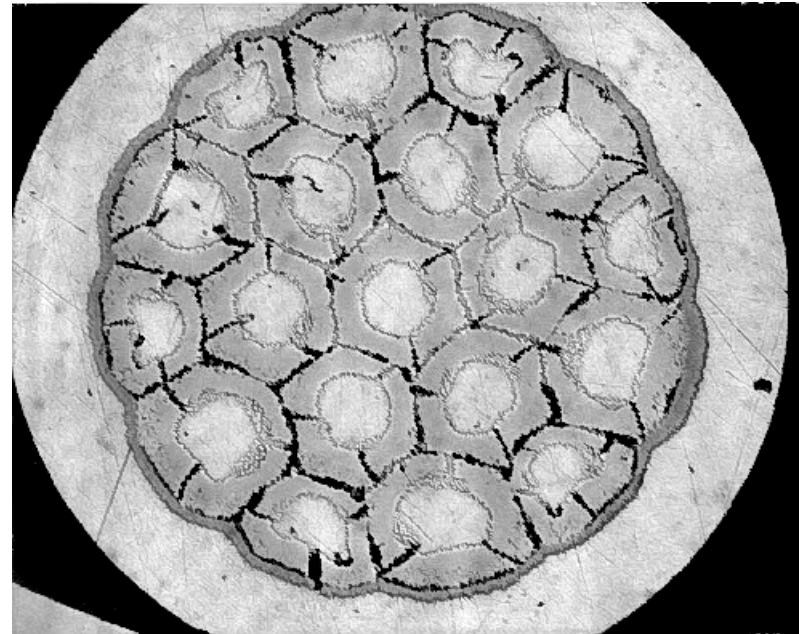
Hentges et al. (OI-ST), ASC 2000





# IGC-AS Program Goals

- Optimize composition to maximize  $J_c$  in internal tin conductor
- Determine optimum split configuration to optimize  $J_c$ /filament size
- Optimize billet design to maximize wire lengths



*3-split sub-elements in 19-stack after reaction (splits are now void regions)*



ADVANCED SUPERCONDUCTORS  
A DIVISION OF INTERMAGNETICS GENERAL CORPORATION

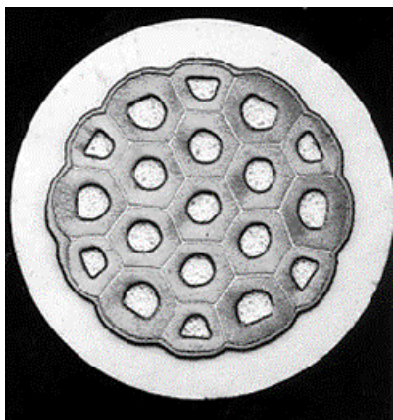
Ron Scanlan ASC2000



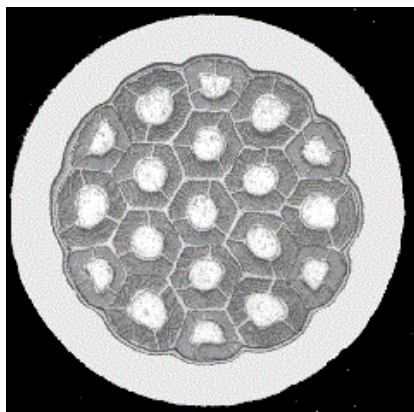


# Summary of IGC-AS Conductor Parameters And Properties

Sample Name	Wire Ø. (mm)	LAR Cu/Nb	# ofSub	J <sub>c</sub> (A/mm <sup>2</sup> ) at 10 <sup>-4</sup> Ω-m & 12T		Q <sub>n</sub> (m J/cm <sup>3</sup> )	D <sub>eff</sub> (µm @5T	Design Composition At. %			Measured Composition			Ø Fil. (µm)
				Non-	Fil.			Cu	Nb	Sn	Cu	Nb	Sn	
LDX	0.6	52/48	19	1140	2917	792	28	62.2	25.9	11.9	--	--	--	5.2
Large Fil. Un-Split	0.6	35/65	37	2200	4622	4860		51.0	33.5	15.5	38.1	39.0	22.0	3.8
Large Fil. 3-Split	0.6	35/65	37	1850	4189	3554	127	54.8	30.7	14.5	47.5	32.1	20.4	3.8
Early Fine Fil	0.6	47/53	19	1950	3924	5621	168	53.4	34.2	12.4	45.7	35.4	16.9	1.4
HD FF 3W-Split	0.8	20/80	19	1768	2993	6544	206	43.5	42.3	14.2	32.0	47.5	20.5	2.3
HD FF 3W-Split	0.7	20/80	19	1910	3233	6547	195	43.5	42.3	14.2	32.0	47.5	20.5	2.0
HD FF 3W-Split	0.6	20/80	19	1906	3231	6142	188	43.5	42.3	14.2	32.0	47.5	20.5	1.7



19-sub-element cross-section of fine filament material 0.6mm Ø strand



19-sub-element cross-section high density 3 split material 0.6mm in diameter

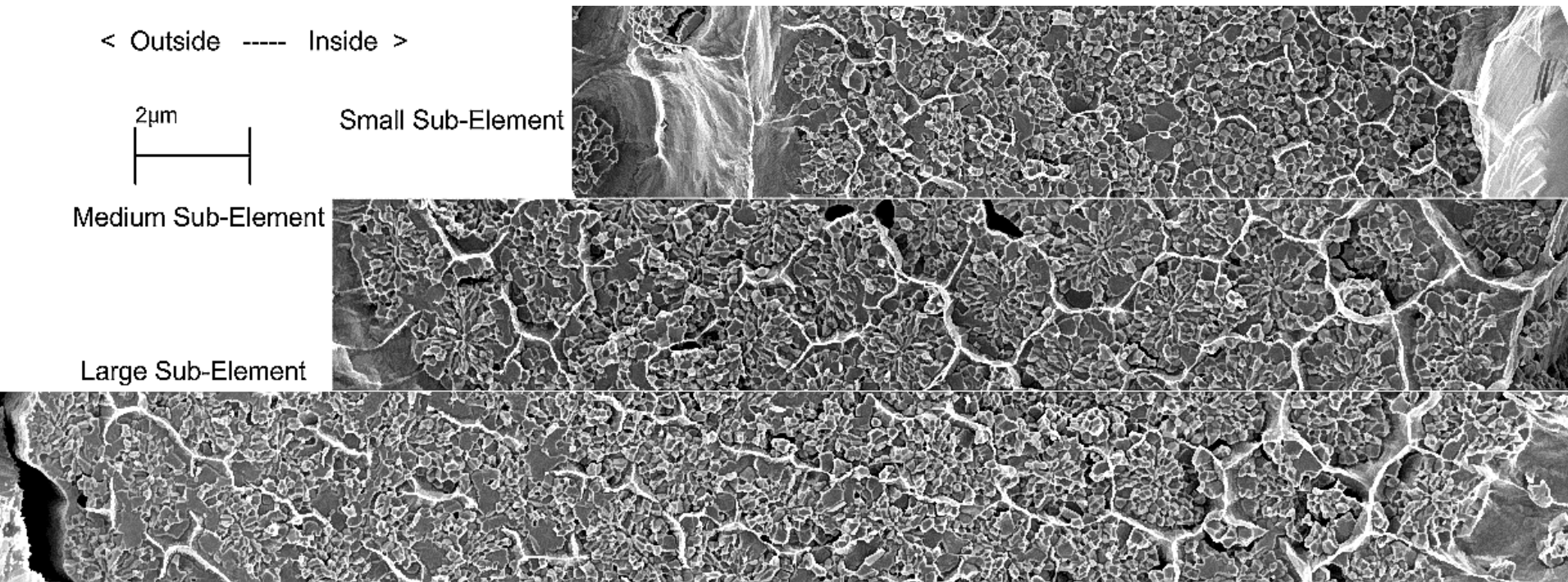
From Taeyoung Pyon and Eric Gregory, ASC 2000







# ***Effect of IGC-AS sub-element size on $\mu$ -structure being measured at the UW***



See  $\mu$ -structure/diffusion effect in layer vs. filament in MJR slide . .

Lee, VLHC Annual Meeting  
2000

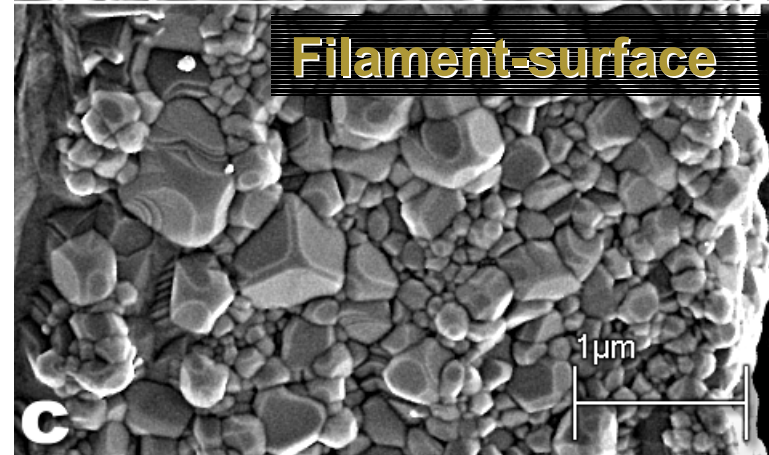
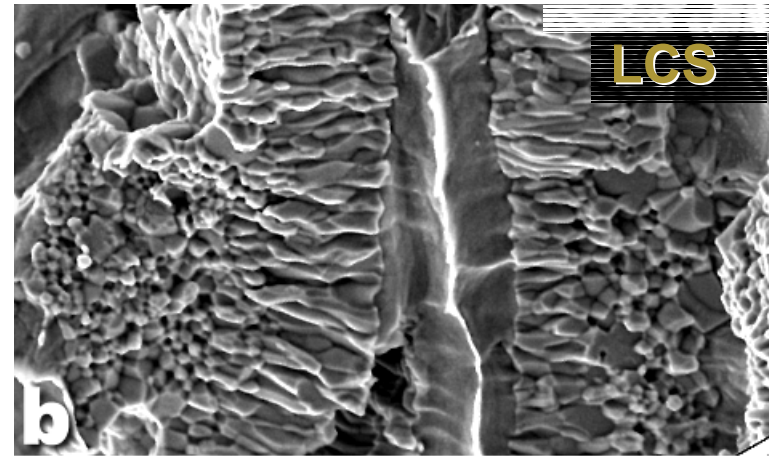
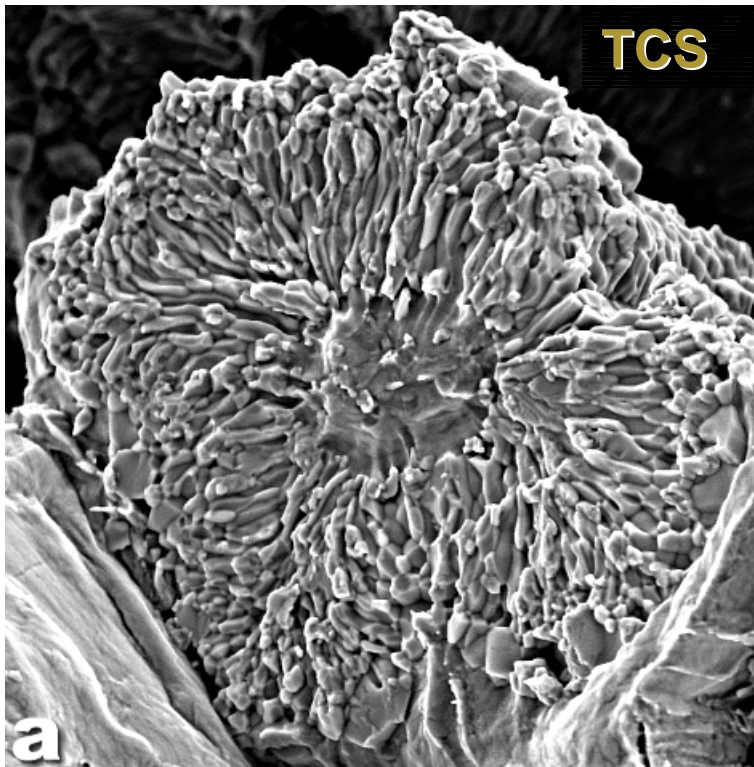




# VAC ITER Standard HT FESEM fractographs

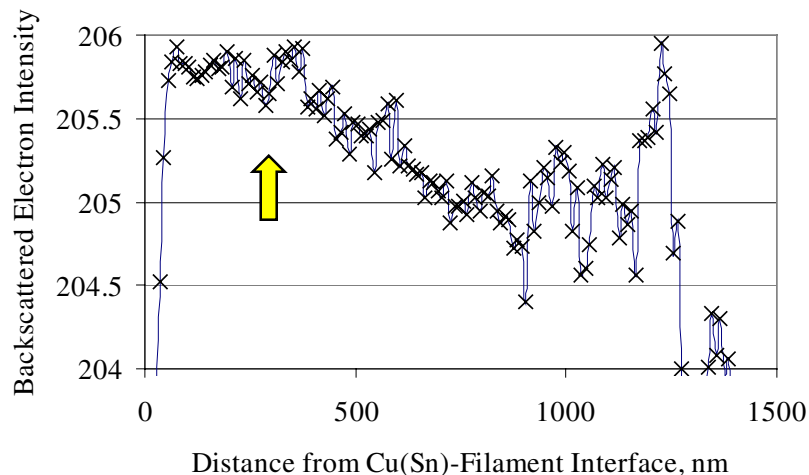
Microstructure  
not exactly  
homogeneous

Lee et al ASC  
2000



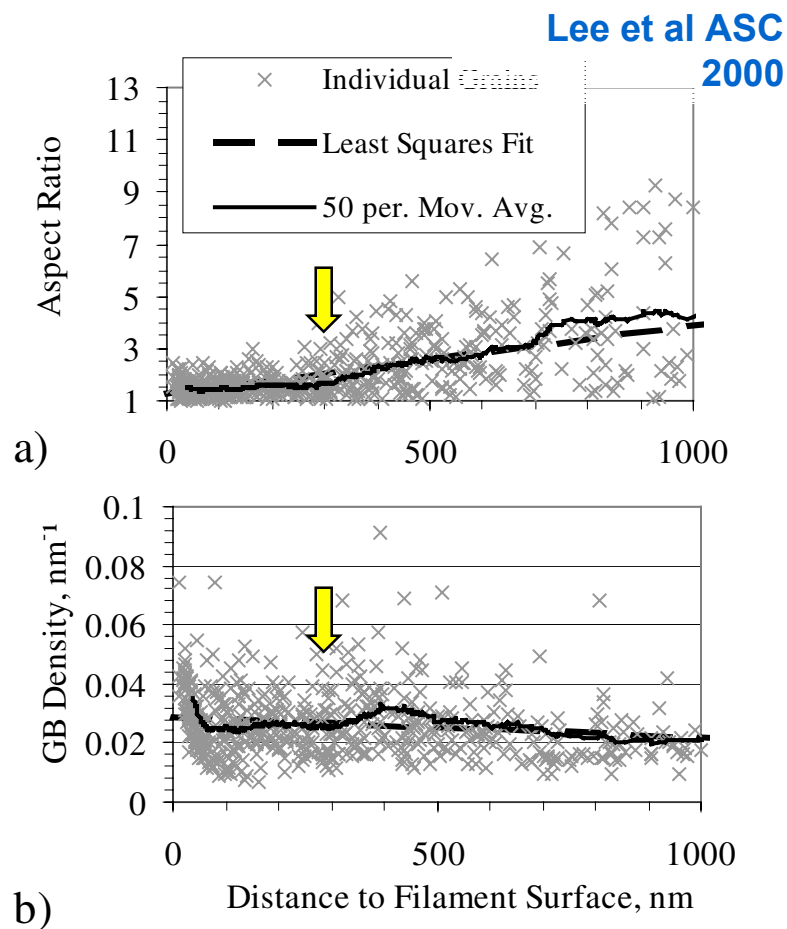


# Chemical and Microstructural Changes At the Same Scale



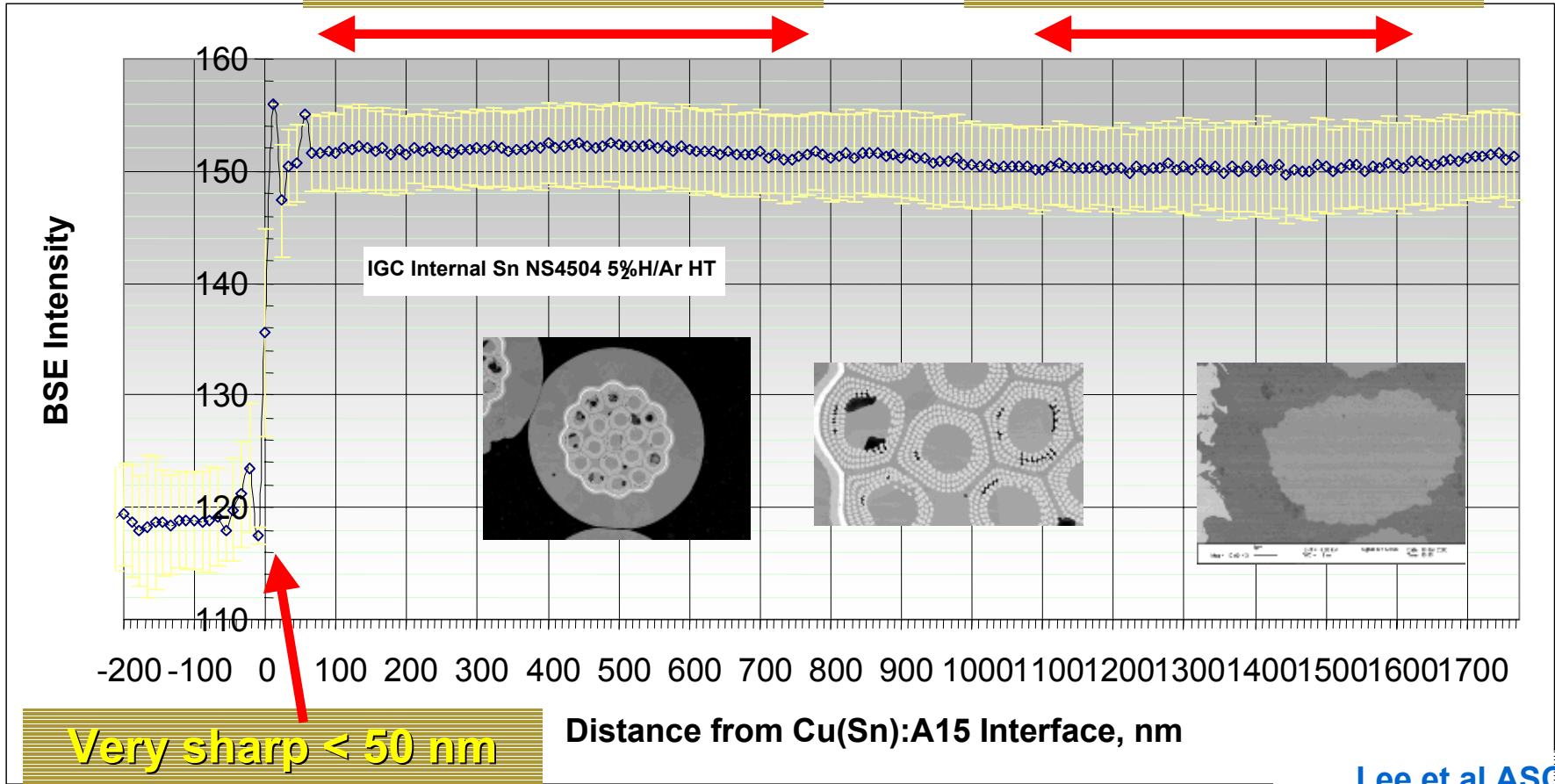
Detail from the traverse in showing a level backscatter intensity up to 300 nm followed by a continuous drop until approximately 900 nm.

Aspect ratio and GB density also show change in behavior at 300 nm



# Example II. IGC ITER Internal Sn Filament (low Sn, low hysteresis loss design)

Plateau 1      Plateau 2



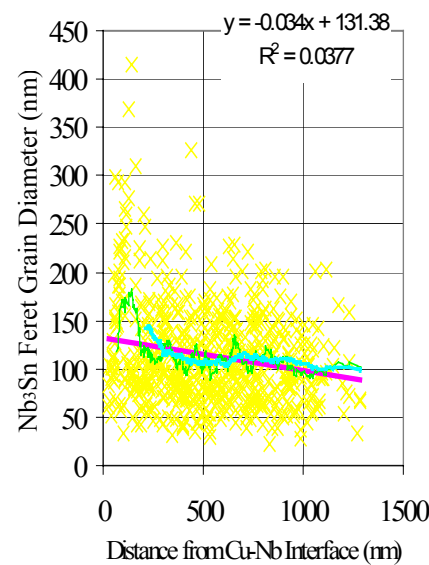
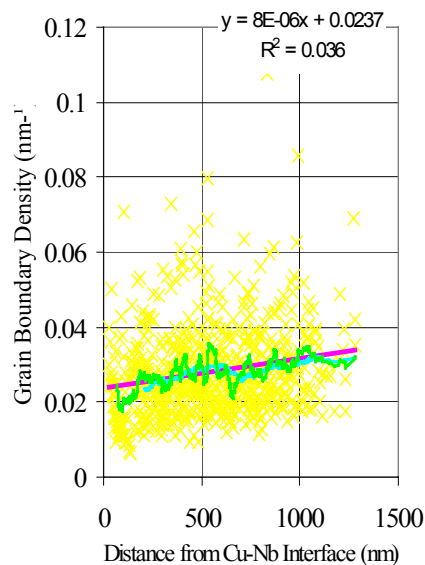
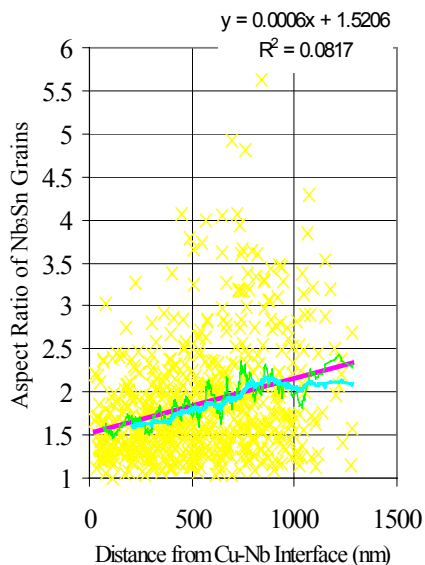
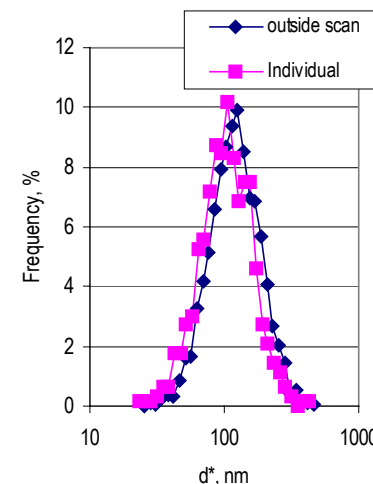
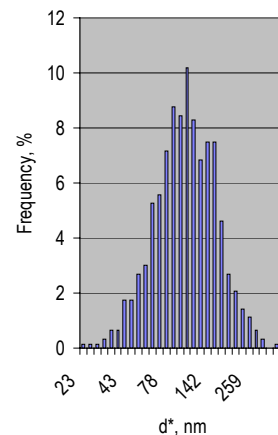
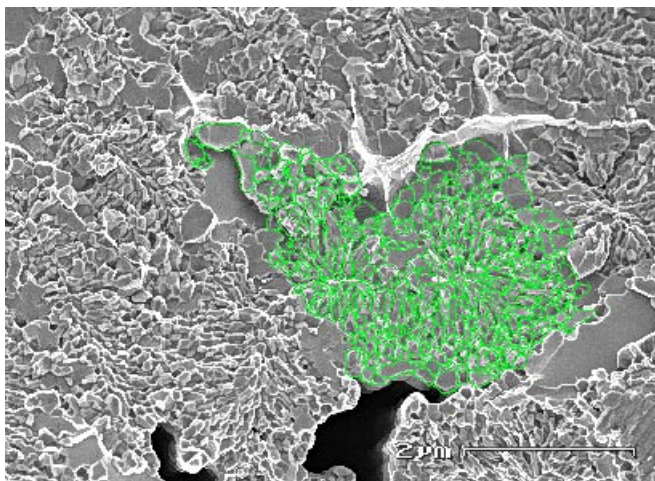
**Very sharp < 50 nm interface**

Lee et al ASC 2000





# TWC 1912 Single filament

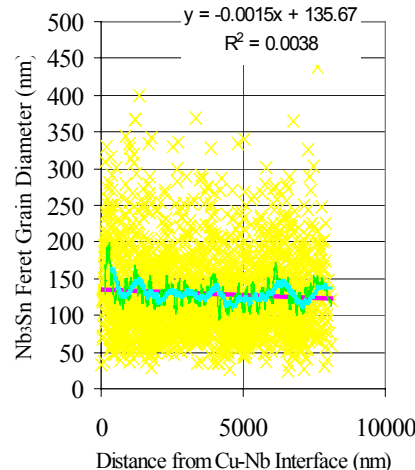
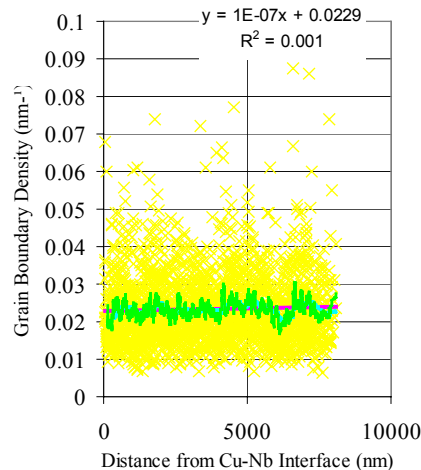
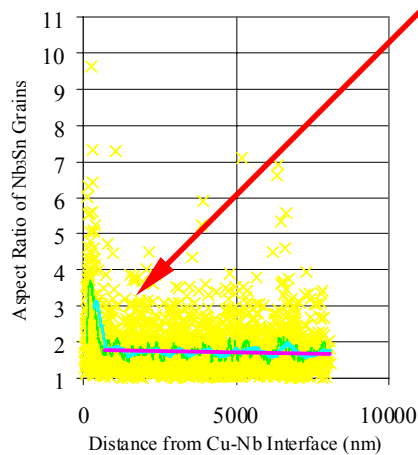
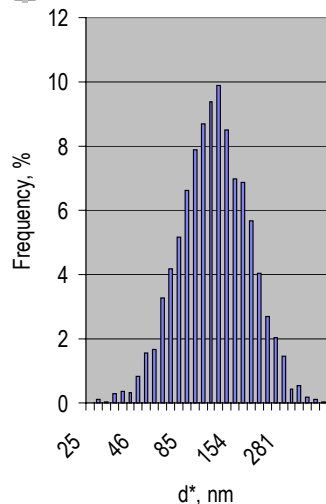
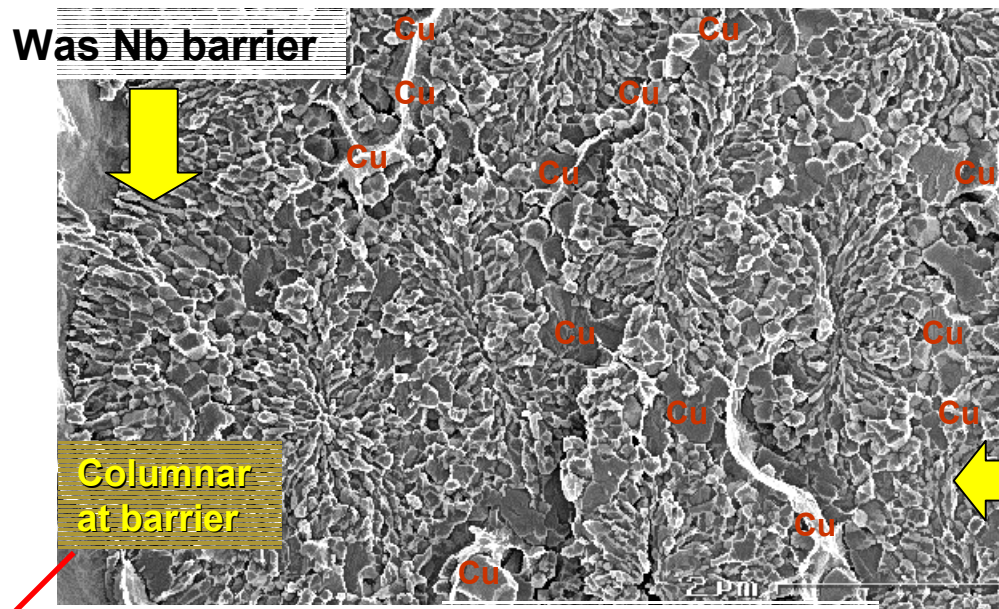


Even with densely packed filaments morphology variations occur across individual filaments.

Lee et al ASC 2000

# CRe1912 overall $\mu$ -structure

Lee et al ASC  
2000

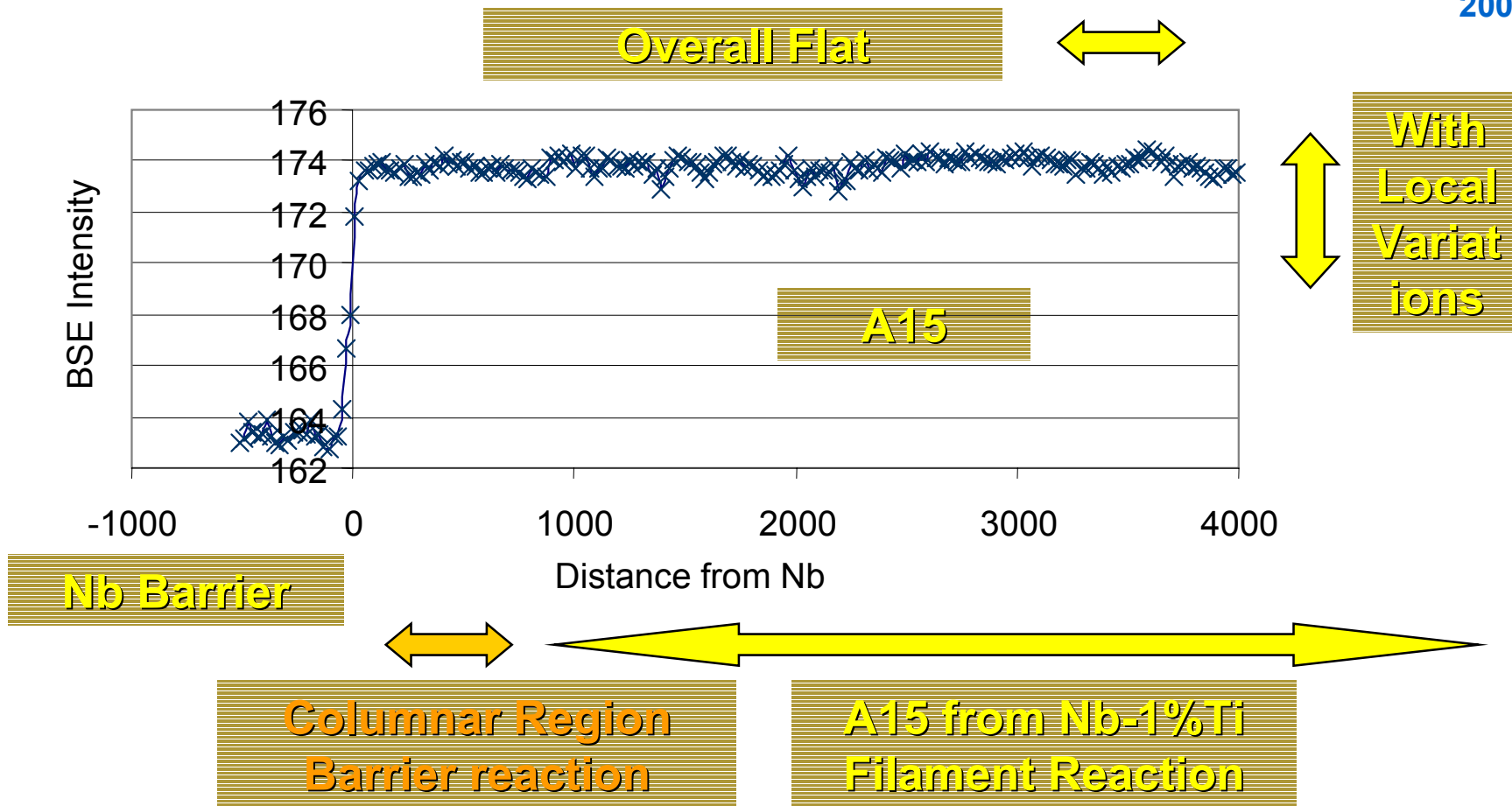


Apart from the columnar grains at the barrier there is a continuous but small morphological variation across the layer in grain boundary density.



# Overall BSE-Composition Across Outer Layer

Lee et al ASC  
2000

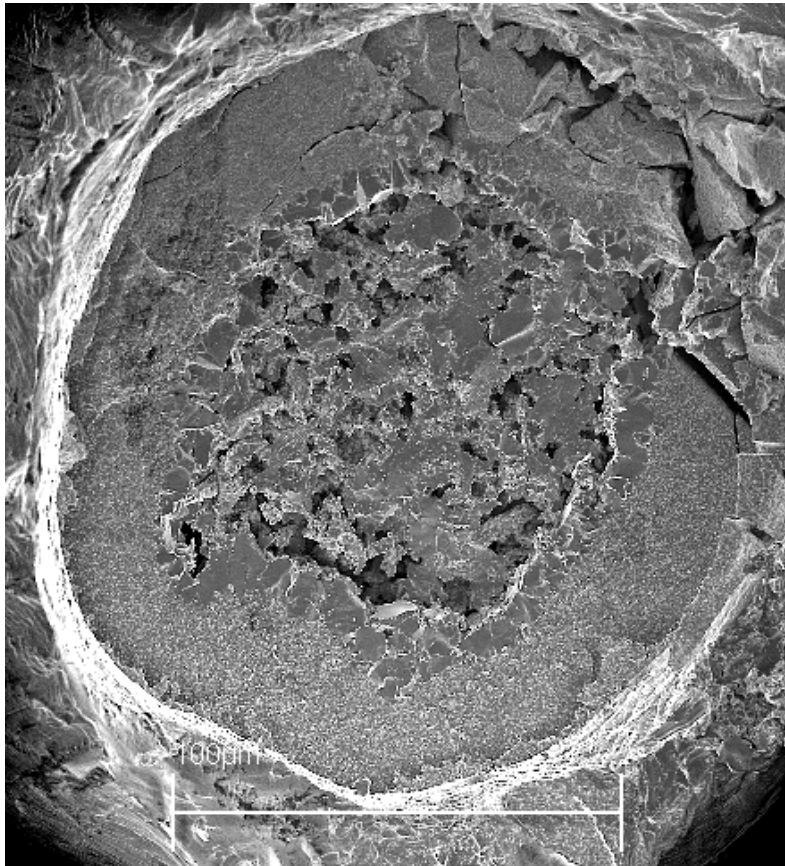




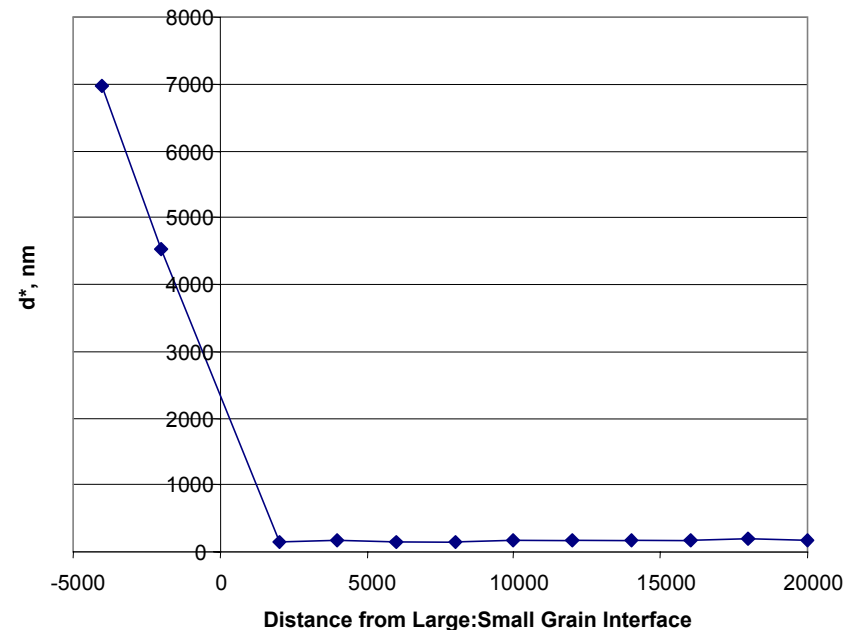
# ECN-Type PIT

## Example of Very High Sn source

Lee et al ASC  
2000



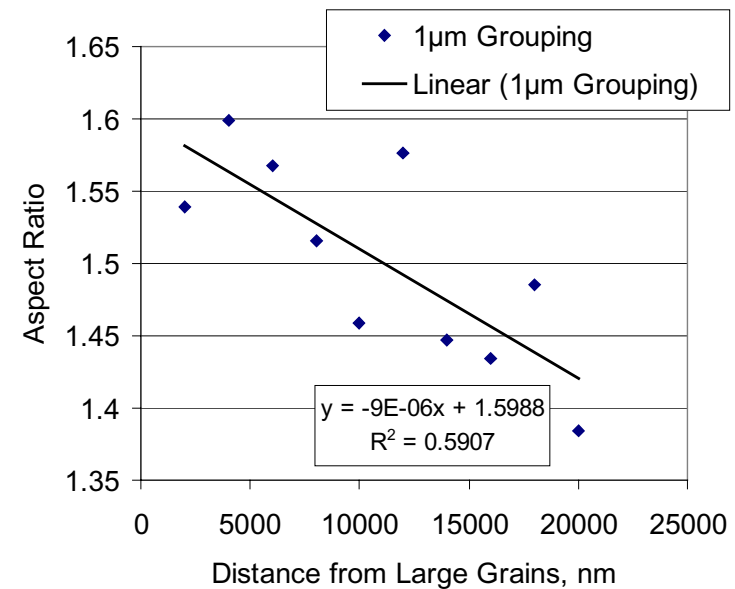
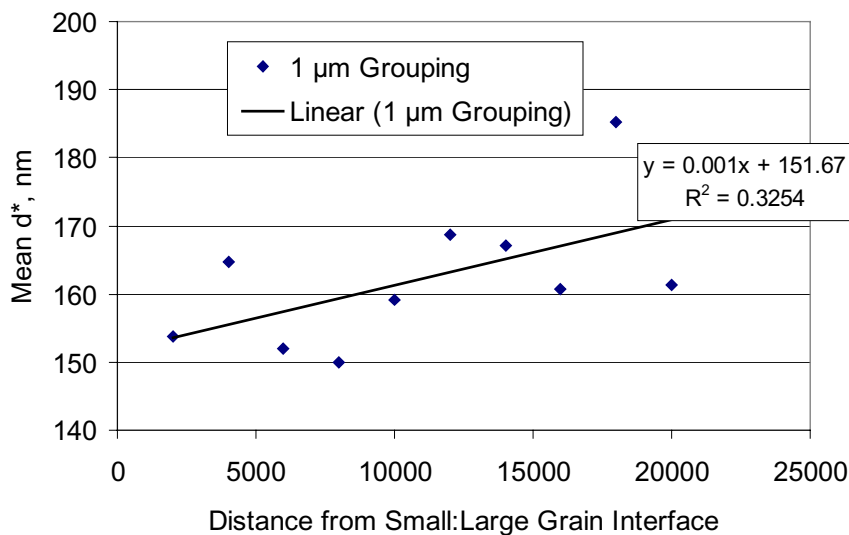
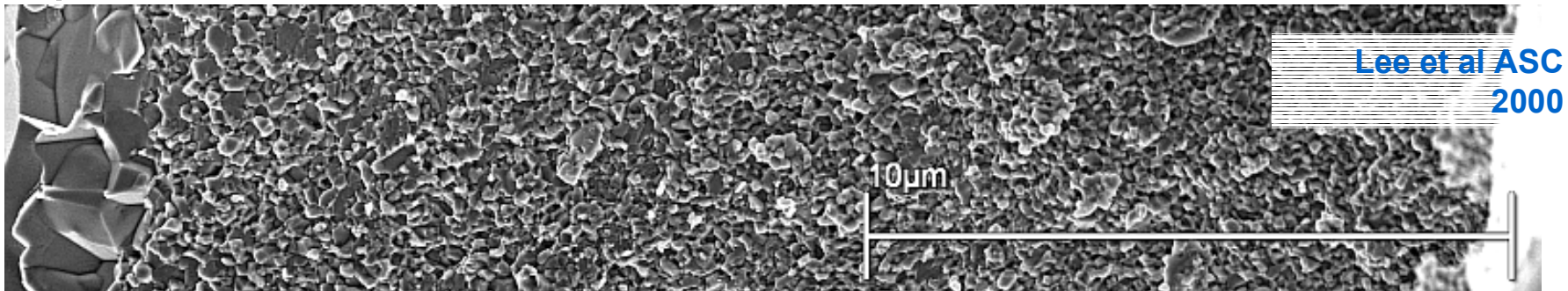
Fracture of Supercon PIT  
Monofilament Reveals inner large  
grain region and outer fine grain region  
around residual powder core







# 20 $\mu\text{m}$ Wide Fine Grain Region



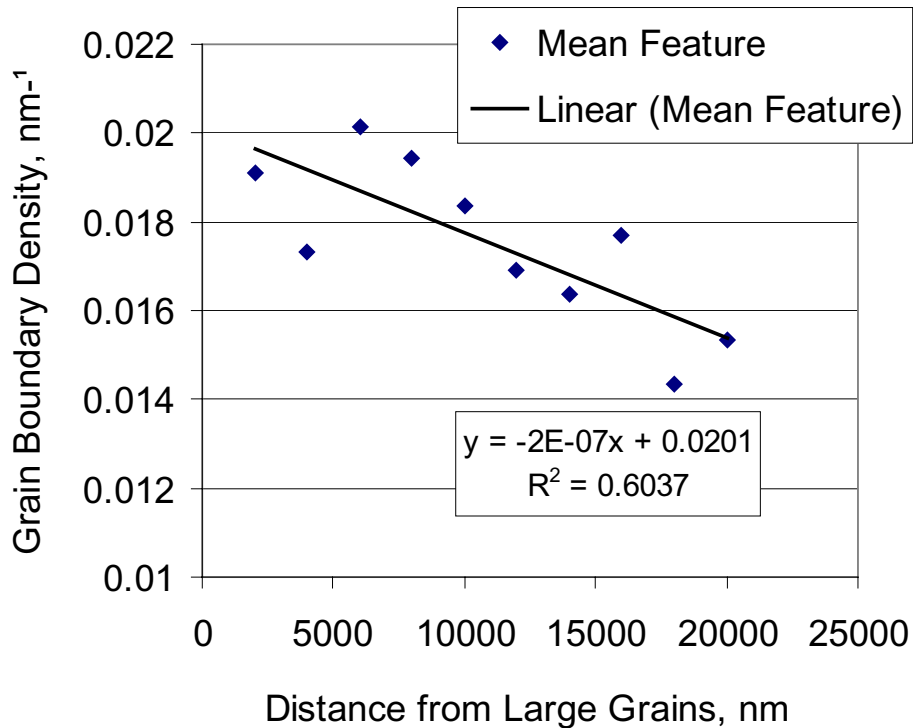
- Shallow gradient in  $d^*$  across layer, surprising aspect ratio gradient



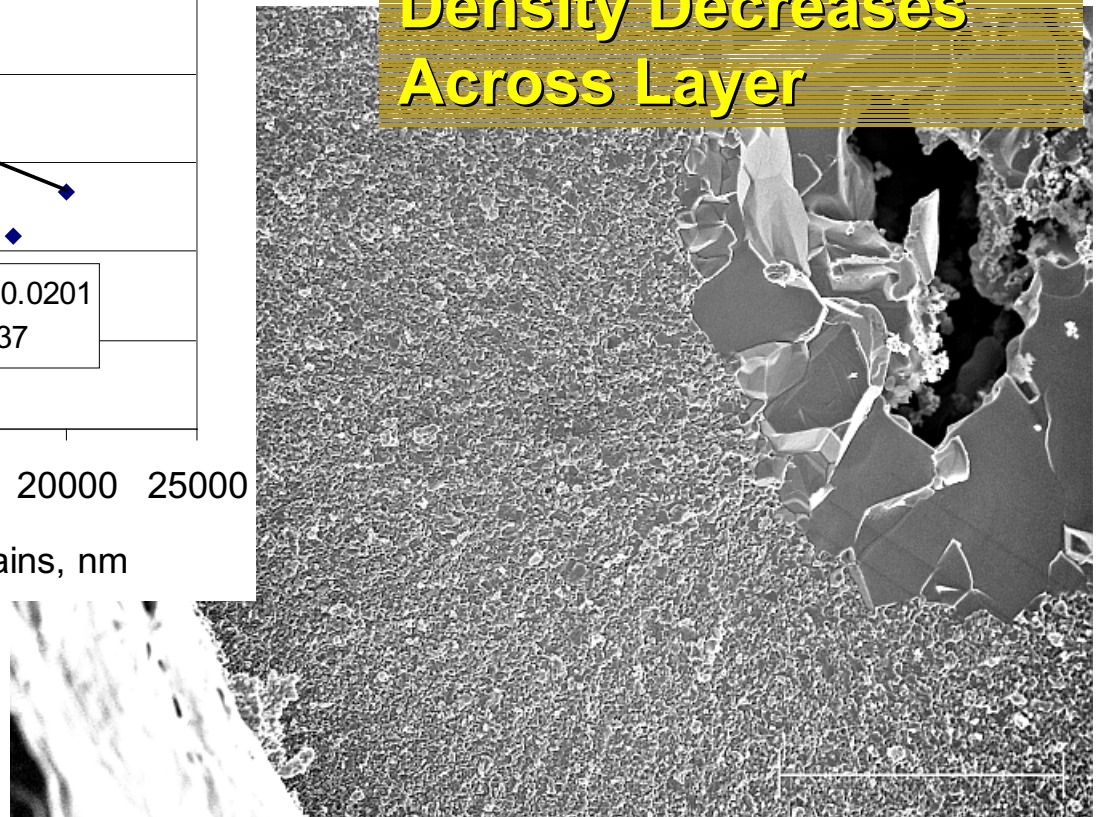


# Grain Boundary Density

Lee et al ASC  
2000



**Grain Boundary  
Density Decreases  
Across Layer**





## ***Recent Microstructure Results***

- In low-Sn internal Sn and bronze-process strand we observe the onset of columnar growth simultaneously with a downturn in %Sn at 300-600 nm into filament.
- In the high-Sn strand we observe that the principal variations are across the original filaments and not across the coalesced filament pack.
- This should impact filament size choice for rod based internal Sn.
- In the ECN style PIT monofilament, with a very high Sn content powder core, a uniform, and fine grain size can be achieved over a very long distance.
- See following results on OI-ST powder route . . .





## ***Cabling work in support of the conductor development program includes***

- Reducing cable  $I_c$  degradation for high  $J_c$  Nb<sub>3</sub>Sn strands
- Understanding the  $J_c$  vs strain behavior for Nb<sub>3</sub>Sn strands made by different processes
- Fabricating new cables designed for react and wind coils
- Exploring cabling alternatives for a more cost-effective conductor

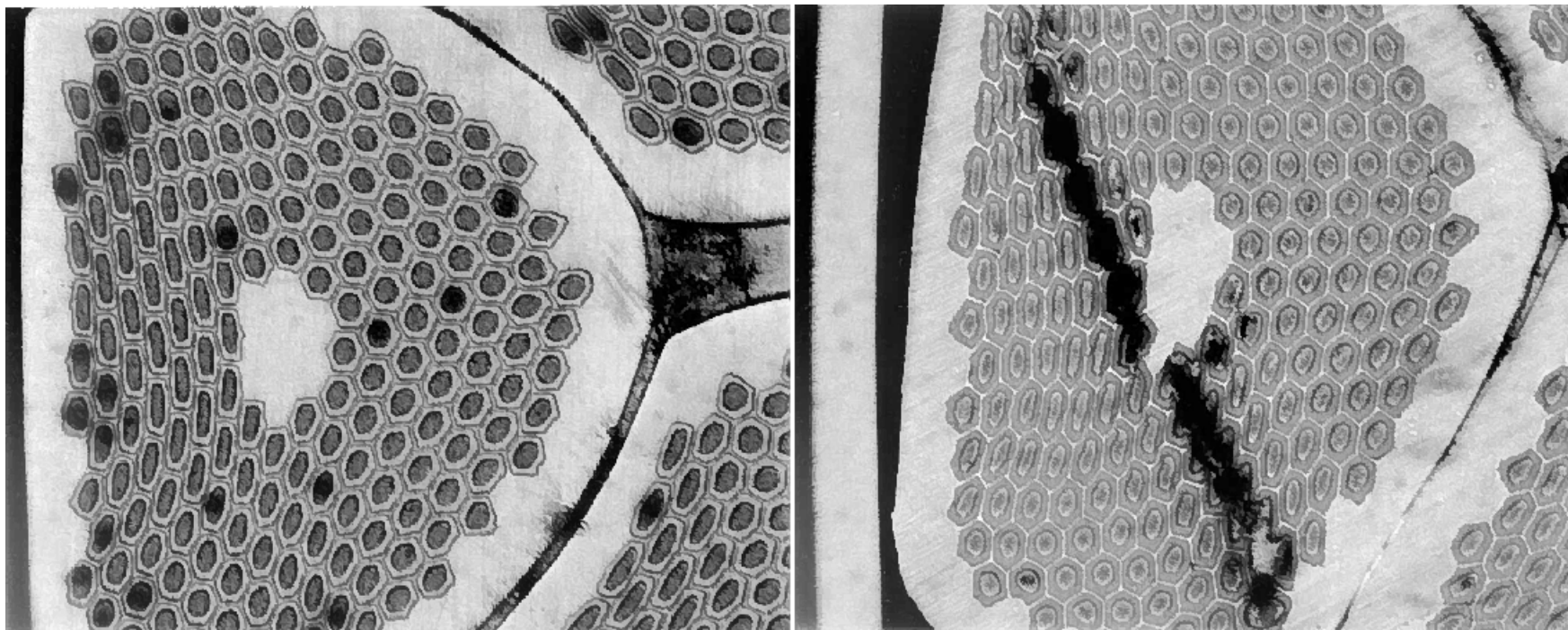


Ron Scanlan ASC2000





# *PIT Nb<sub>3</sub>Sn strands at edge of Rutherford cable*



*Moderately compacted*



*Highly Compacted*





# PIT strand Chronology from Twente

pre-print of paper 4LB-02, presented at the Applied Superconductivity Conference, Virginia Beach, September 2000

TABLE II  
CHRONOLOGICAL SUMMARY OF THE PIT-CONDUCTOR DEVELOPMENT PROGRAM

PIT wire	$J_c$ non-Cu @ 10 T, 4.2 K (A/mm <sup>2</sup> )	Cable performance
<u>1998</u>		
ECN binary 192	2200	40 $\mu$ m filaments
SMI binary 492	1890	$J_c$ too low
SMI binary 504 (1)	2650	damaged filaments
<u>1999</u>		
SMI binary 192	2700	damaged filaments
SMI ternary 192	3200	damaged filaments
<u>2000</u>		
SMI binary 504 (2)	2200	OK
SMI ternary 504	2800	OK

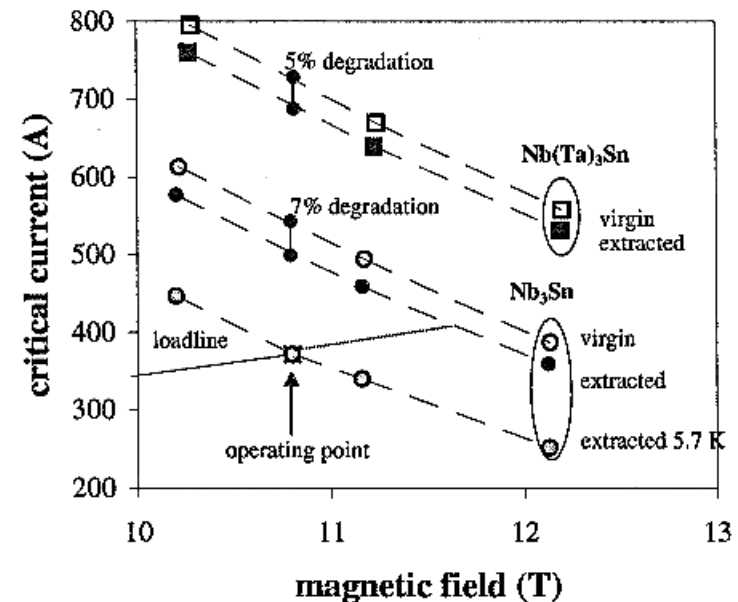


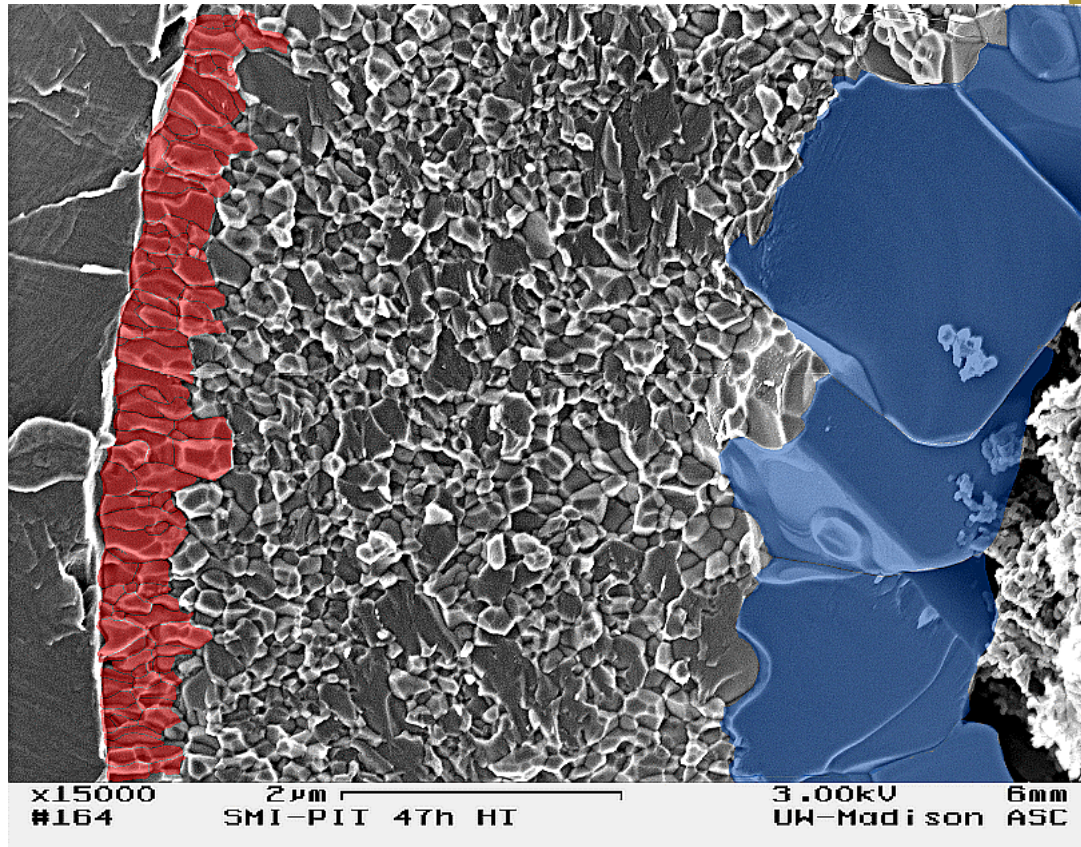
Fig. 1. Critical current at 4.2 K of binary and ternary PIT-Nb<sub>3</sub>Sn conductors as a function of the self-field corrected applied magnetic field of both virgin wires and extracted strands. Also shown is the predicted critical current of the binary extracted strand at 5.7 K.

Andries den Ouden et al. ASC2000





# Analysis of Layer $J_c$ and $Q_{gb}$ in non-alloyed SMI-PIT strand



In this partial fracture cross-section of a SMI-PIT strand, three distinct grain size/morphology regions are observed.

- Columnar adjacent to the Nb
- Fine equiaxed center
- Very large grains adjacent to core.

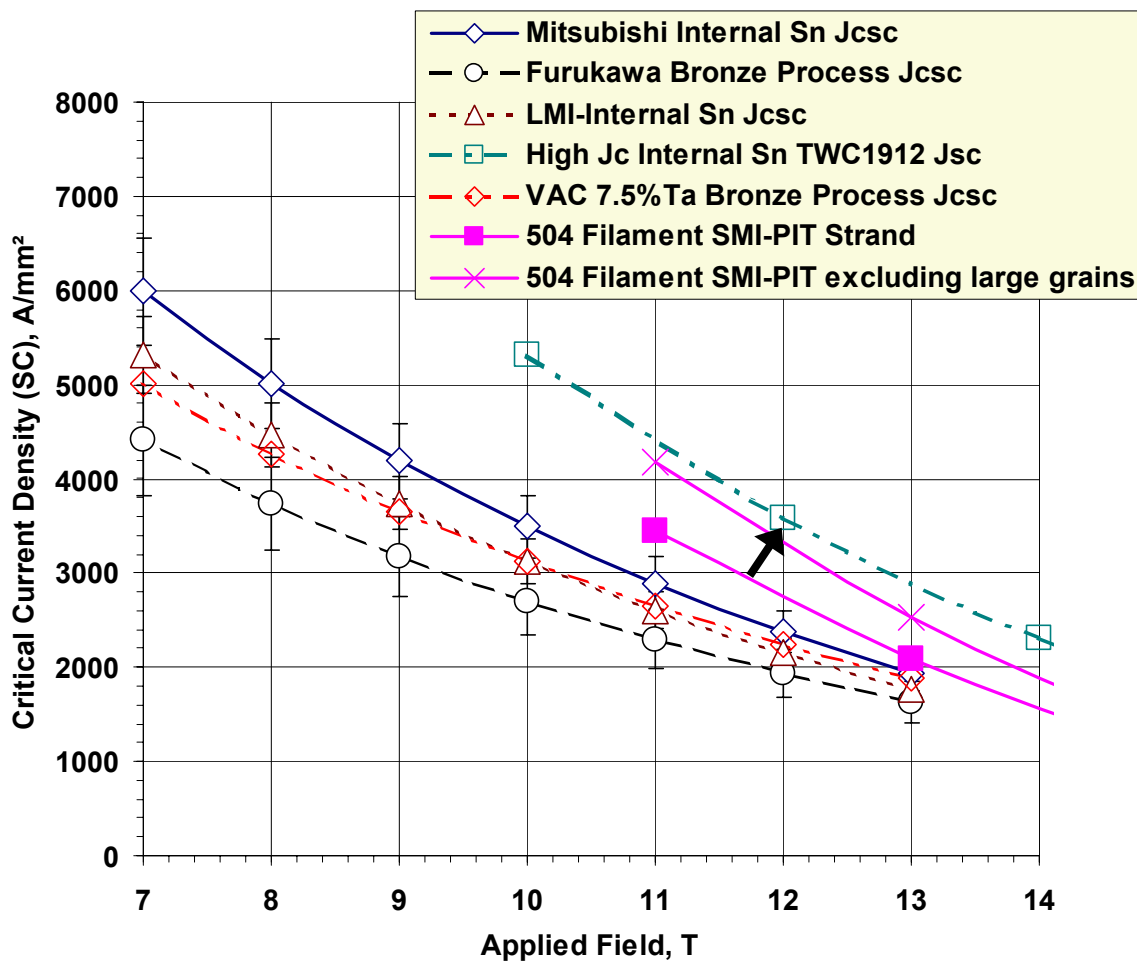
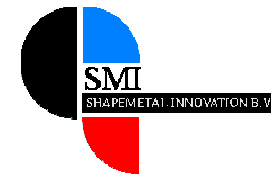
If the very low grain boundary density in the large-grain area means that this area does not contribute significantly to  $I_c$  then we can adjust the  $J_{csc}$  data to reflect the “good” area.

Lee et al. (UW)





# Non-Alloyed SMI PIT $J_{csc}$



Lee et al. (UW)

When the  $J_{csc}$  data is calculated excluding the non-contributing large grain area the performance of the PIT A15 more closely matches the high  $J_{csc}$  internal Sn strand.

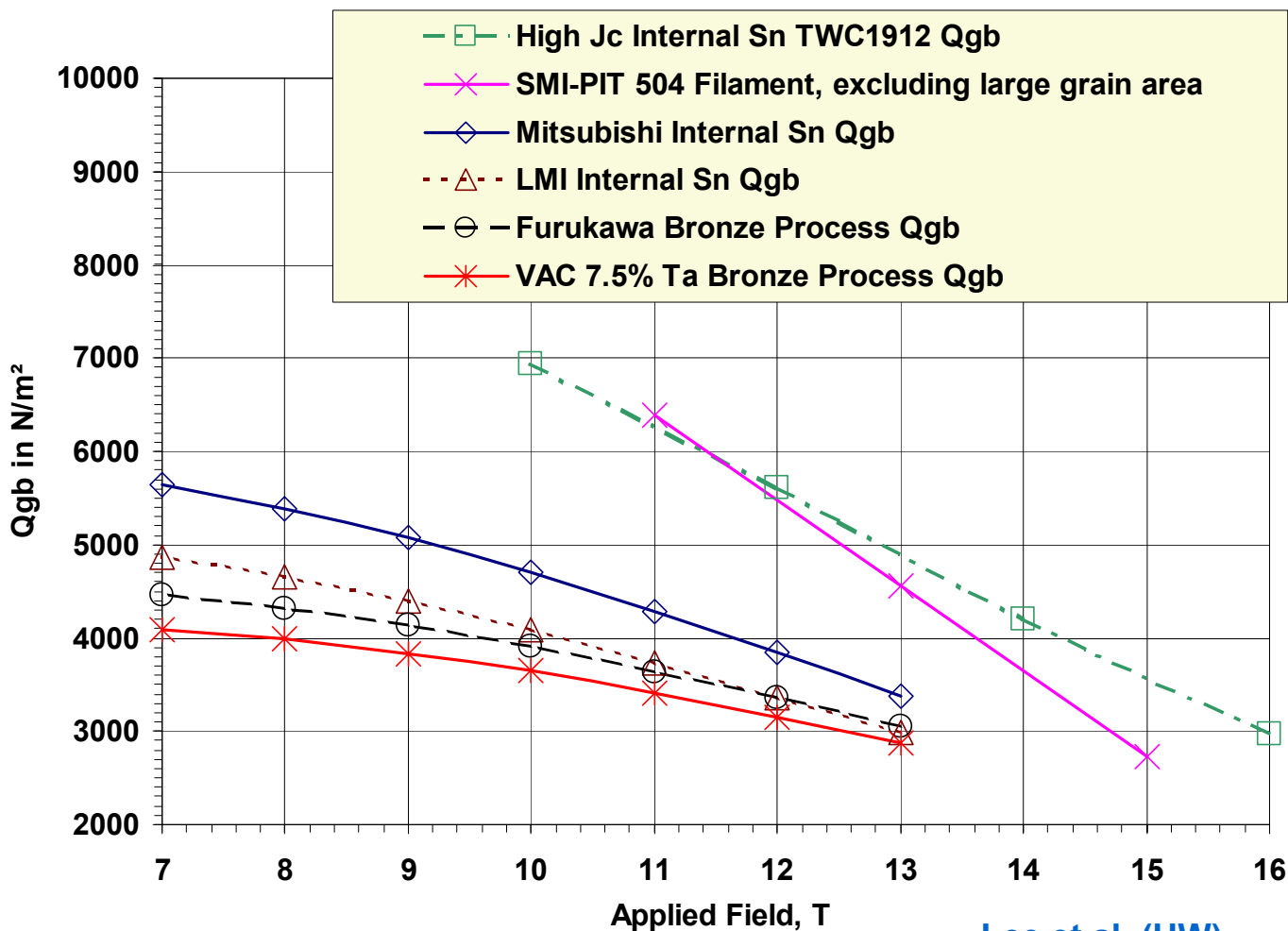
The higher  $J_c$  of the new  $Nb(Ta)_3Sn$  can be expected to increase the  $J_{csc}$  further







# Specific Grain Boundary Pinning Comparison



Lee et al. (UW)

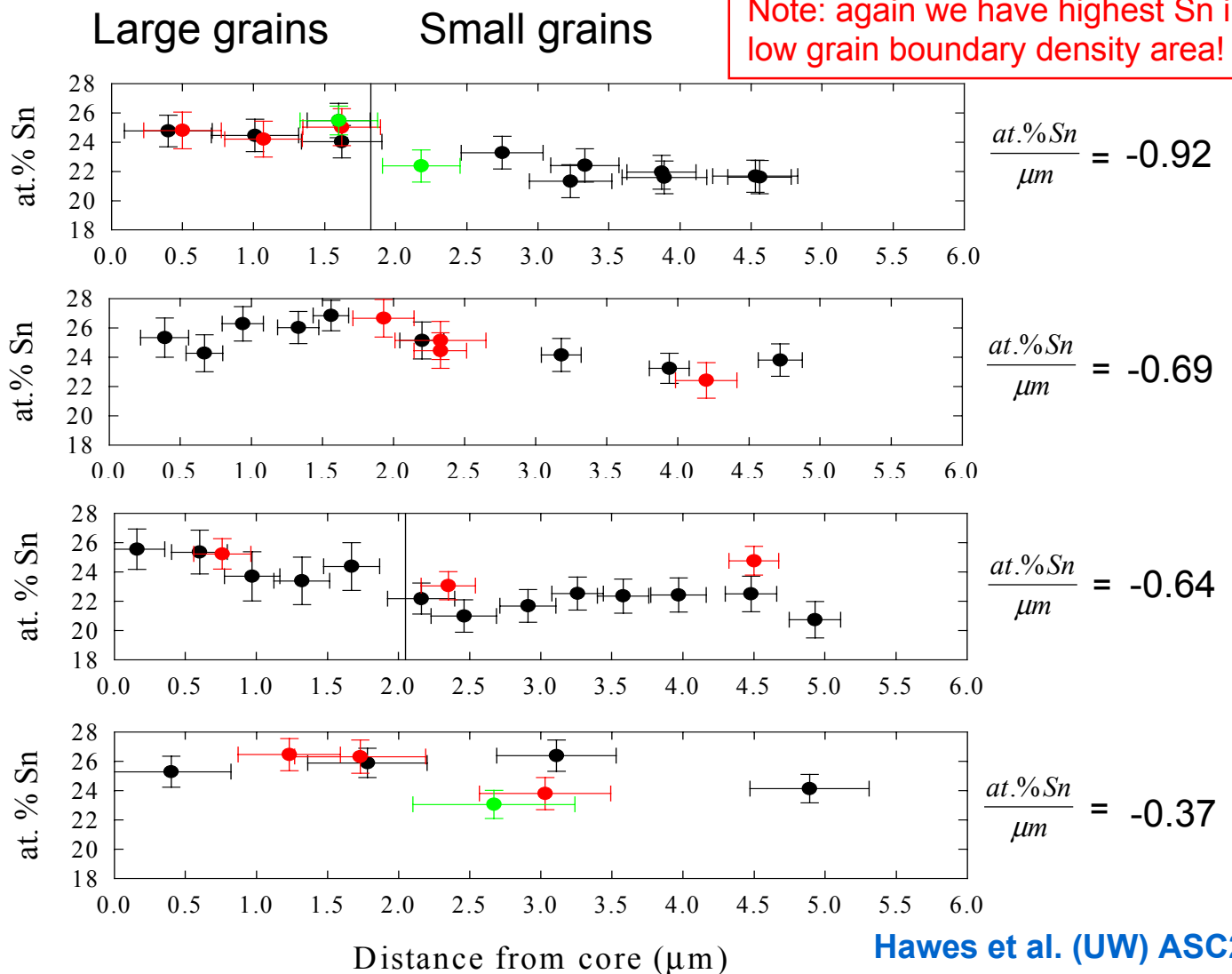
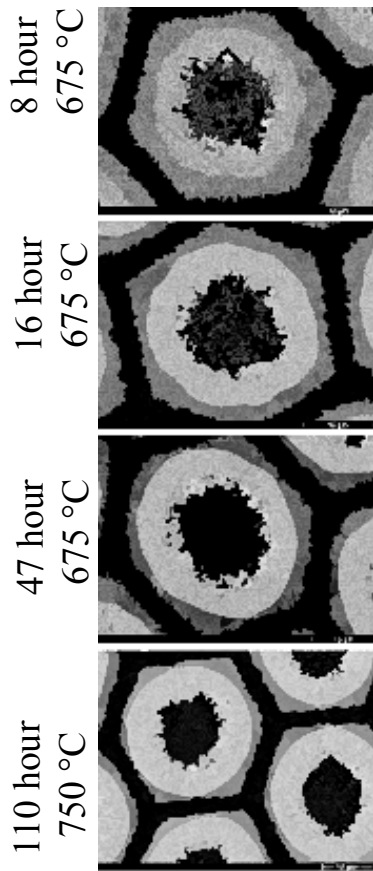
High Sn and PIT strands have 50% higher  $Q_{gb}$  (and  $J_{csc}$ ) than ITER style strands

The new  $Nb(Ta)_3Sn$  PIT should not have the high field tail off observed here.



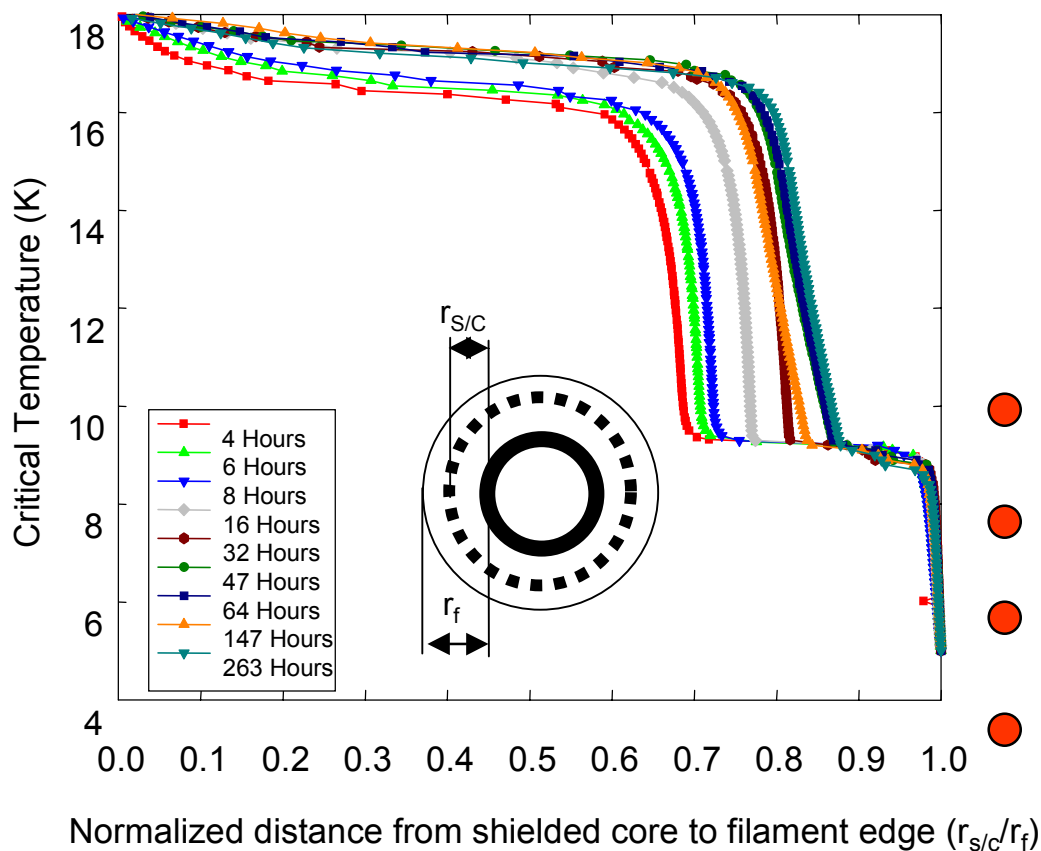
# EDX Measurements

Note: again we have highest Sn in low grain boundary density area!





# 675 °C $T_c$ Profiles in SMI PIT



- The  $Nb_3Sn$  in PIT filaments has progressively higher Sn into the filament from the barrier, thus the change in properties through the layer can be analyzed without the shielding that occurs in bronze and internal Sn filaments.
- 4-8 hr plots have a steeper slope.
- Layer growth visible.
- After 32 hrs growth rate slows.
- Tail appears at ~ 14 K after 47 hour HT.

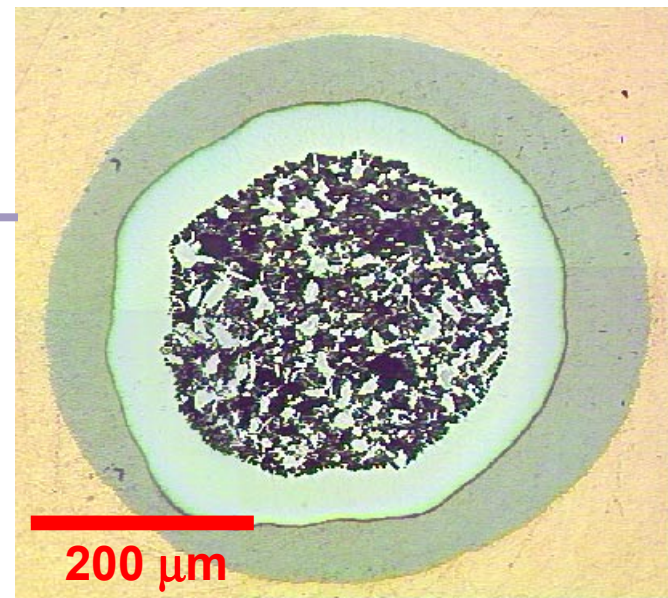
Hawes et al. (UW) ASC2000





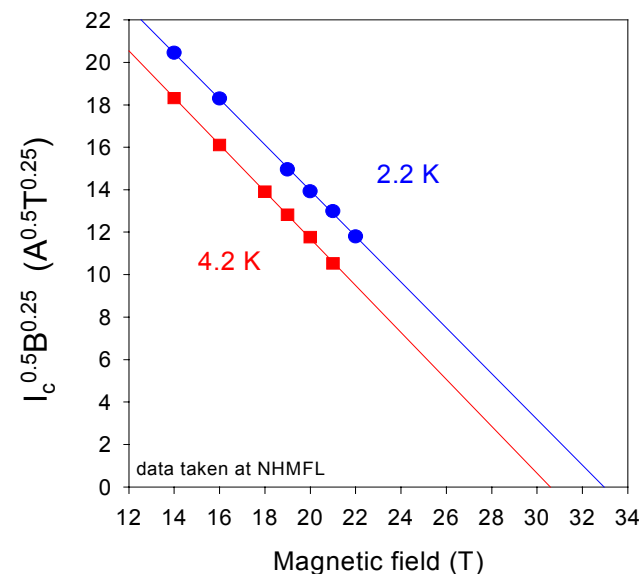
# Powder-in-tube $\text{Nb}_3\text{Sn}$ development at OI-ST

- Ta+Sn+Cu mixed together, similar to Tachikawa et al. process (ASC'98)
- thick  $(\text{Nb,Ta})_3\text{Sn}$  layers
- high  $\text{Nb}_3\text{Sn}$  layer  $J_c$
- high  $B_{c2}$



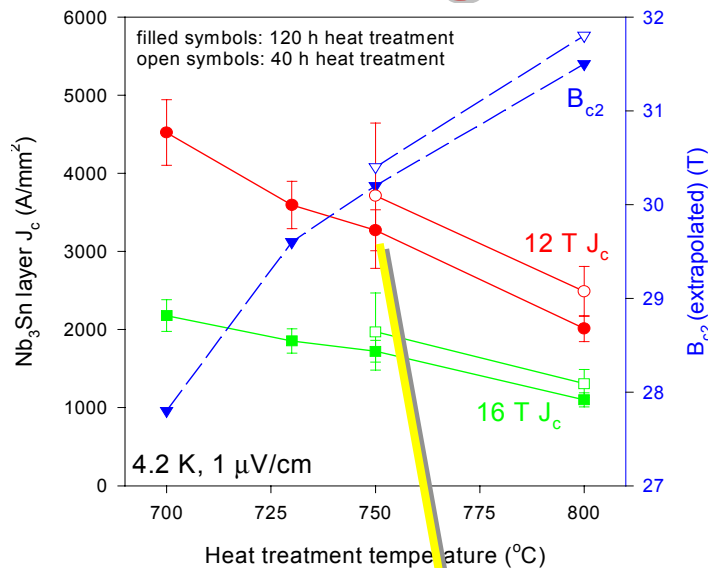
OXFORD

Hentges et al. (OI-ST), ASC 2000



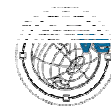
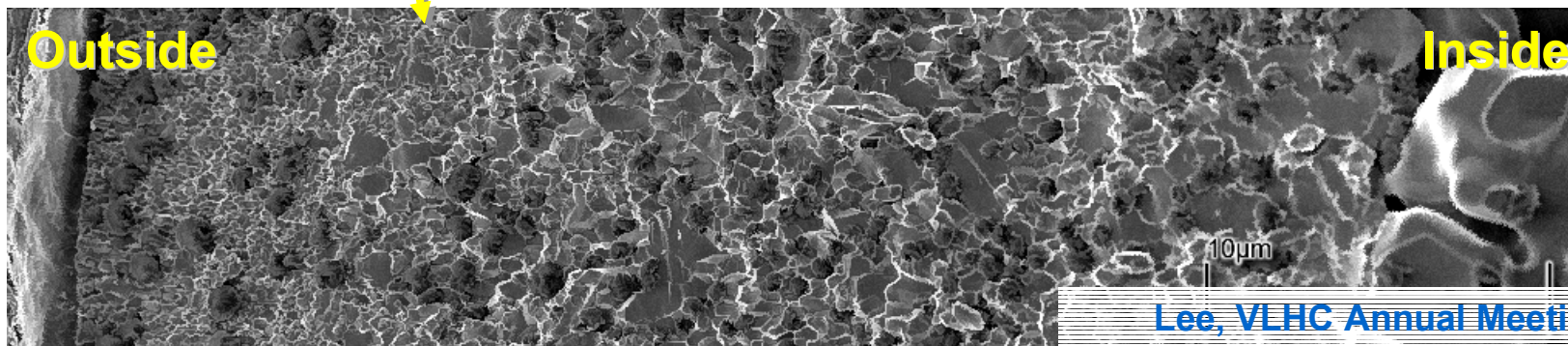


# $\mu$ -Structure from UW shows fine enough grain size for pinning and high Kramer extrapolation



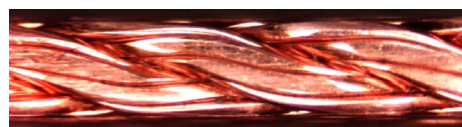
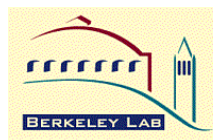
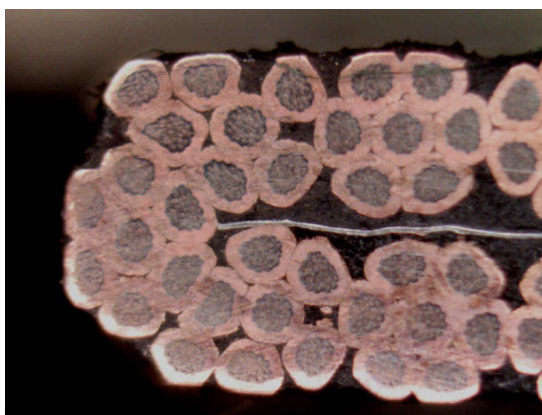
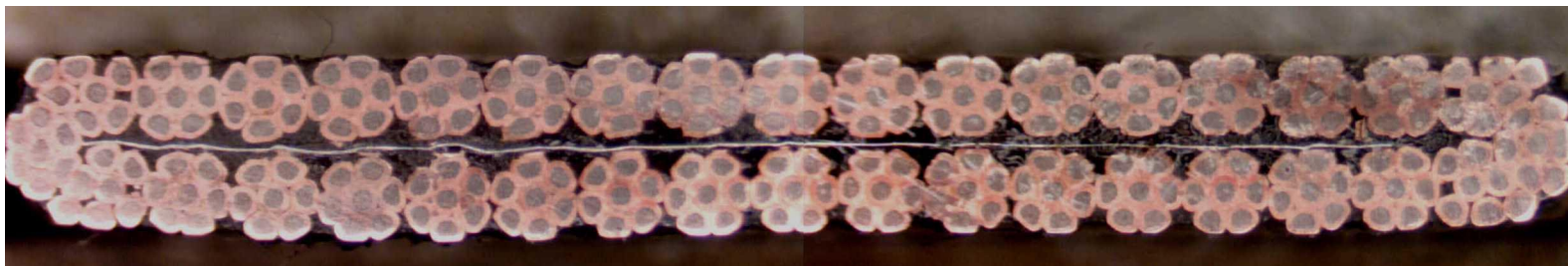
The effect of heat treatment on  $J_c$  and  $B_{c2}$  for PIT wire.  $B_{c2}$  data is extrapolated from 16 T.

Note grain size gets smaller towards the outside.

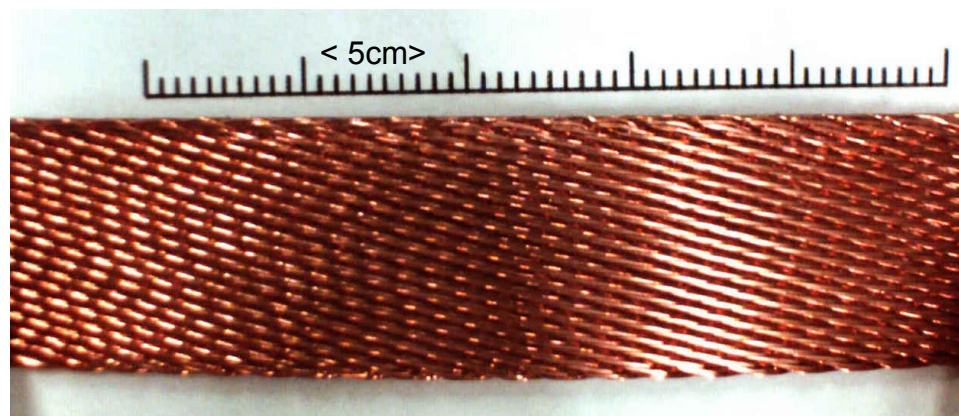
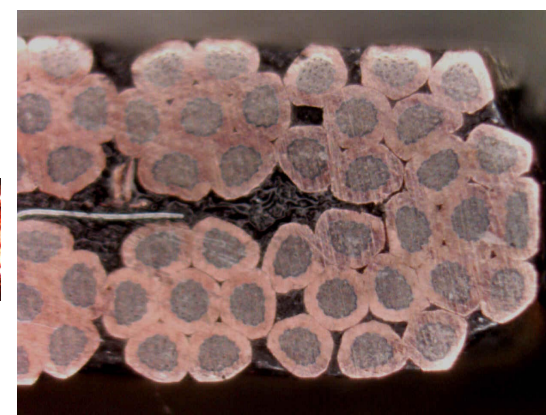




# FNAL R&W R3I-00741a Mfg. LBNL 2/17/00 **6-in-1 Cabling**

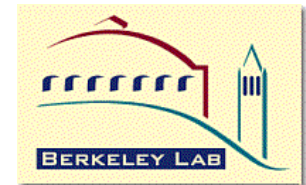
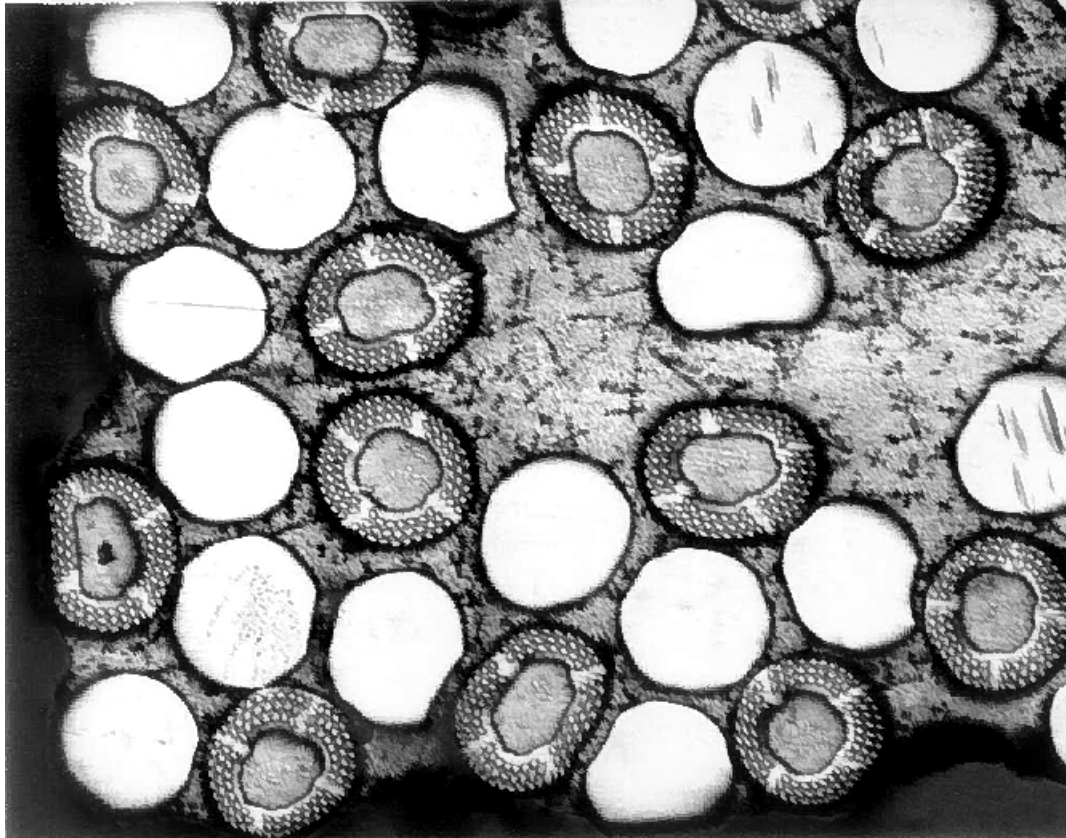


**Ron Scanlan ASC2000**





# ***Rutherford cable made from sub-cables with 4 copper and three superconductor strands***



Ron Scanlan ASC2000





# ***A High Current Density Low Cost Niobium<sub>3</sub>Tin Conductor Scaleable to Modern Niobium Titanium Production Economics MEIT Approach***

- To meet the VLHC target one has to
  - Increase current density by adding niobium and tin at the expense of copper
- Reduce cost by designing a process that can be manufactured in large scale 450kg billets
  - eliminate barrier?, lower cost barrier,

**Zeitlin (Supergenics), Gregory and Pyon (IGC-AS), ASC 2000**





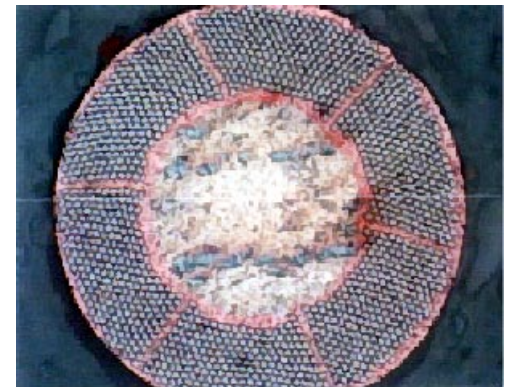


# *Design Approach*

- Single element composite for fabricability
- Fine filaments to speed reaction and decrease grain size
- Segmented to reduce loss
- Minimize composite copper thus boosting tin and niobium
- Evaluate need for barrier

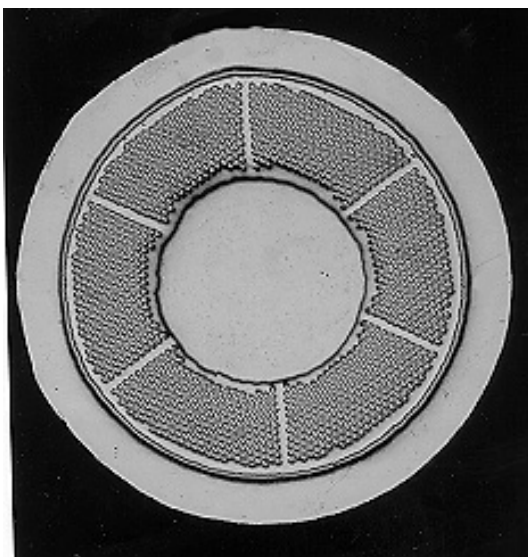
Zeitlin (Supergenics)  
Gregory and Pyon (IGC-AS)  
ASC 2000

BAZ1 six  
segment wire  
0.142mm





# Conductor Configurations



Cross Section Before Reaction

Zeitlin (Supergenics)  
 Gregory and Pyon (IGC-AS)  
 ASC 2000

<b>Billet, 178mm</b>	<b>BAZ1 6 seg.</b>	<b>BAZ2 3 seg.</b>
<b>Filament #</b>	<b>1434</b>	<b>1475</b>
<b>Nb: area% / At%</b>	<b>31.7/28.0</b>	<b>32.7/29.1</b>
<b>Sn: area% / At%</b>	<b>27.1/16.1</b>	<b>27.1/16.2</b>
<b>Cu: area% / At%</b>	<b>41.2/55.9</b>	<b>40.1/54.7</b>
<b>Bronze At%</b>	<b>22.4</b>	<b>22.8</b>

<b>Reduced Sn</b>	<b>BAZ1 6 Seg.</b>	<b>BAZ2 3Seg.</b>
<b>Nb: area% / At%</b>		<b>29.5/24.9</b>
<b>Sn: area% / At%</b>		<b>22.2/12.6</b>
<b>Cu: area% / At%</b>		<b>48.3/62.5</b>
<b>Filament Size at 0.14 mm</b>	<b>1.9 μm</b>	<b>1.9 μm</b>
<b>Segment Size at 0.14 mm</b>	<b>22x55 μm</b>	<b>22x110 μm</b>





# MEIT Fabrication Results



**179 mm 1434 filament Billet**

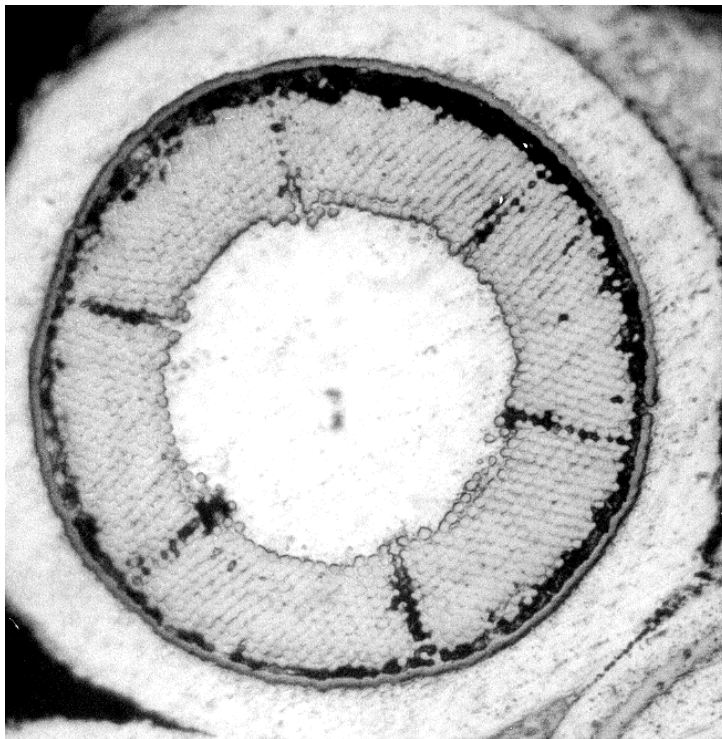
- Fabrication and wire drawing
  - Processing was smooth,
    - ◆ one break at 1.5 mm , mechanical
  - 10000 and 30000 meter lengths at 0.14 mm
    - ◆ Break was mechanical, commercial wire draw
- Barrier required at high tin
  - could engineer barrier free but  $J_c$  would suffer

Zeitlin (Supergenics), Gregory and Pyon (IGC-AS), ASC 2000

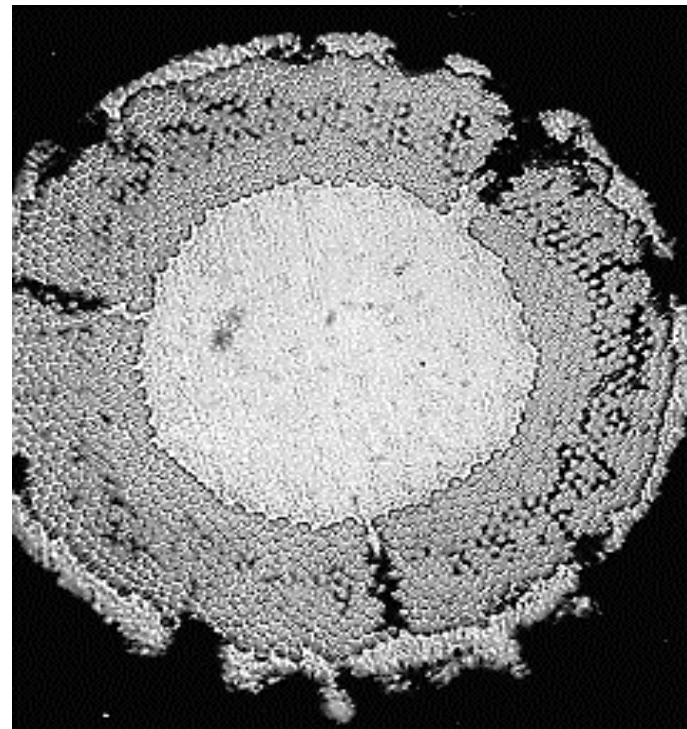




# Reacted Cross Sections



TaBrBaz1 Tantalum Barrier  
0.2mm



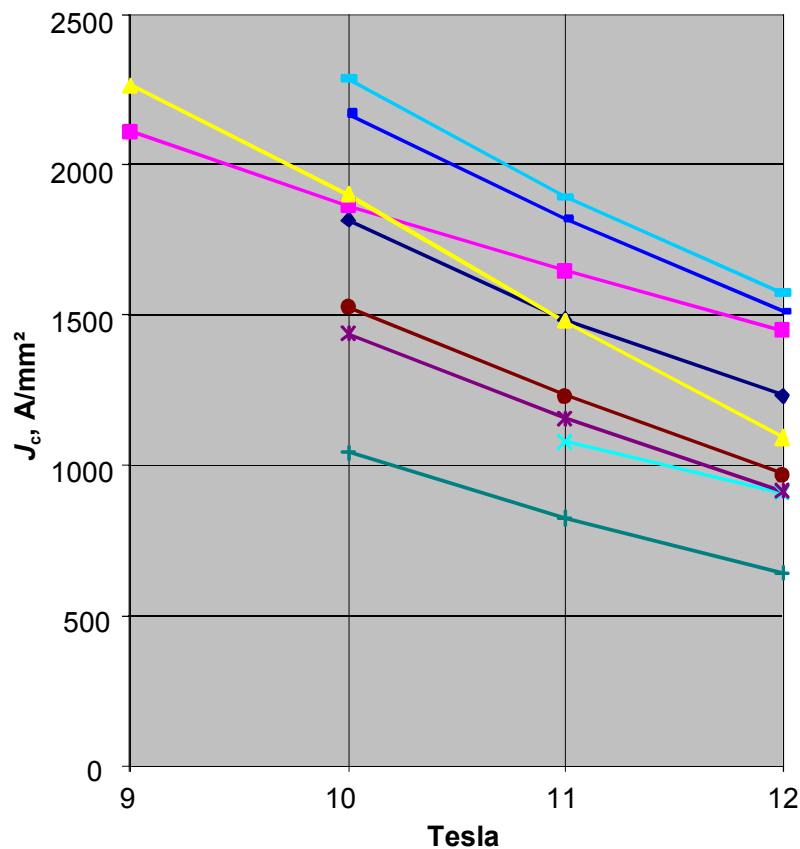
BAZ2A lower tin 0.20 mm

Zeitlin (Supergenics), Gregory and Pyon (IGC-AS), ASC 2000





# Test Results



	Cable ID	Barrel# Heat Treat	Wire Size mm	Filament µm	Comment
	BAZc101	688 - C	0.60	0.9	19 TIB
	BAZb101	682 - B	0.60	0.9	19 TIB
	TaBBAZ1	220 - A	0.20	1.9	TIB
	TaBBAZ1	216 - A	0.30	2.8	Ta Integ Barrier (TIB)
	TaSBAZ1	224 - A	0.14	1.4	TIB
	BAZ2A	227 - A	0.20	2.8	SB
	BAZ2A	206 - A	0.29	4.0	SB
	TaBarAll	229 - A	0.29	2.8	TIB
	BAZ1-2-1	201 - A	0.29	4	Separated Barrier (SB)

Data from Zeitlin (Supergenics), Gregory and Pyon (IGC-AS), ASC 2000





# Test Results

- 19 element 0.9  $\mu\text{m}$   $J_c$  normalized to Nb  
5400-5500  $\text{A}/\text{mm}^2$  at 12 T  
– 650  $^\circ\text{C}$  240 hrs
- Mono element with barrier (MEIT), 2  $\mu\text{m}$   
filament 4800  $\text{A}/\text{mm}^2$
- MEIT at 1.4  $\mu\text{m}$  less 3600- over-aged?  
– 700  $^\circ\text{C}$  24 hrs.

Zeitlin (Supergenics)  
Gregory and Pyon (IGC-AS)  
ASC 2000





# ***Cost Model Assumptions by Supergenics***

- Full scale 300 mm dia. billet as per table
- Two production volumes, 300 and 12000 tonnes
- 400 % and 300% overhead rate with 40% GM
- Material prices as quoted from suppliers
- Barrier introduced at later stage of processing  
- semi to continuous clad

Zeitlin (Supergenics)  
Gregory and Pyon (IGC-AS)  
ASC 2000





# ***Design Elements of Full Scale Billet***

	<i>Full Scale Billet</i>	<i>Clad Niobium</i>
Extrusion Billet	300 mm dia. x 810 mm length	250 mm dia. x 610 mm length
Copper Clad Nb Hex Rod	3.2 mm	200 mm
Tin Alloy Core	2.6 mm	
Filament #	4614	1
Nb/Sn/Cu %	36/24/49	66.4
Yield	85% - 429 kg	94% - 239 kg

**Zeitlin (Supergenics), Gregory and Pyon (IGC-AS), ASC 2000**







# MEIT Cost Model Results

0.25mm core@300 %OH	$J_c$ A/mm <sup>2</sup> 12 T	Price \$/m Nb <sub>3</sub> Sn	Price \$/m cable	Price \$/kAm
5%Ta Bar	2000/3000	0.12	0.50	1.23/0.82
2.5%TaB	2000/3000	0.10	0.42	1.06/0.71
5% Ta40Nb	2000/3000	0.11	0.46	1.12/0.75
2.5% Ta40Nb	2000/3000	0.10	0.40	1.00/0.67

Zeitlin (Supergenics), Gregory and Pyon (IGC-AS), ASC 2000





# ***MEIT Conclusion***

- Target costs and performance for VLHC appear feasible
  - MEIT conductor promises to be easy to fabricate
    - ◆ Low cost cladding technique still to be developed
    - ◆ SnTi alloy has to be commercialized to lower cost
  - Layer  $J_c$  of 5500 A/mm<sup>2</sup> with 50% Nb could yield 2750 A/mm<sup>2</sup> at 12 T
    - ◆ Need to improve understanding of layer current density and additives - build margin

Zeitlin (Supergenics)  
Gregory and Pyon (IGC-AS)  
ASC 2000





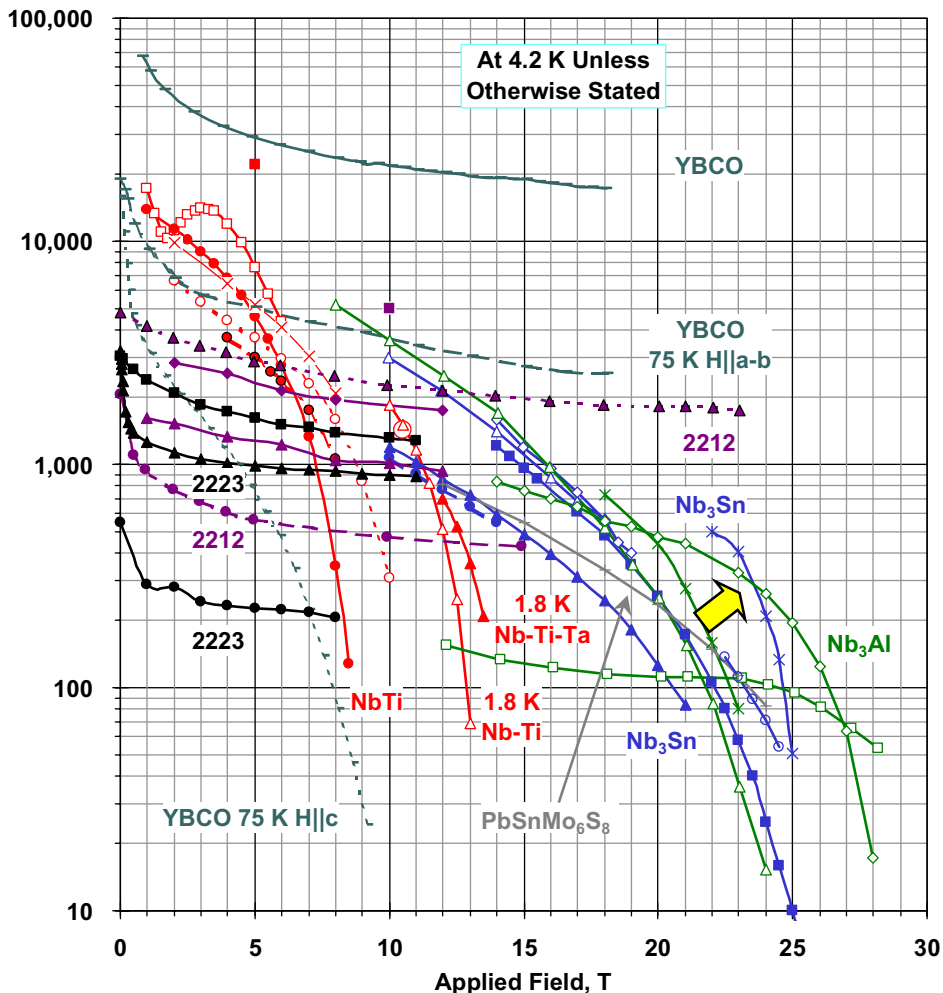
# ***Rapid quench process Nb<sub>3</sub>Al has advanced significantly this year.***

- Best material has similar  $J_c$  at 12 T, 4.2 K, A-15 area to MJR Nb<sub>3</sub>Sn
- Major advances this year relate to the super high field needs of 1 GHz NMR (23.5 T @ 1.8 K)
  - DRHQ shows dramatic  $J_c$  improvement at > 20 T
    - ◆ D = 2nd RHQ treatment added
    - ◆ 1st RHQ - Synthesis of Nb-Al Supersaturated solution
    - ◆ 2nd RHQ - phase transformation to A15 Nb<sub>3</sub>Al
- New TRUQ process has greater potential for cladding and cabling than older RHQ processes. After quenching it has a ductile bcc supersaturated solid solution. “Transformation-heat-based up-quenching.”



# DRHQ process from NRIM shows further potential of Nb<sub>3</sub>Al

Critical Current Density, A/mm<sup>2</sup>

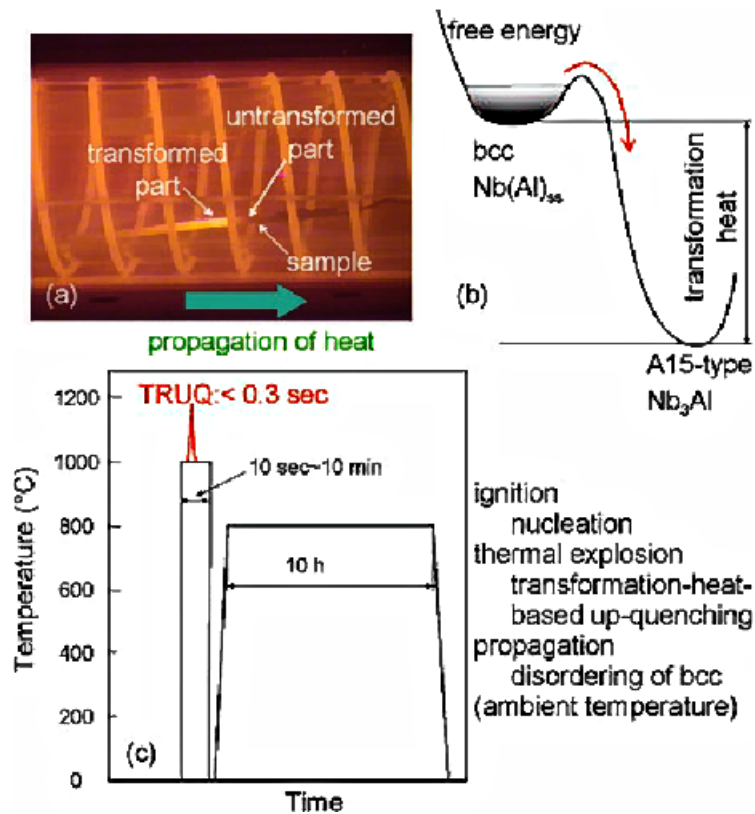


- Nb-Ti: Nb-Ti/Nb (21/6) 390 nm multilayer '95 (5°), 50 μ V/cm - McCambridge et al. (Yale)
- Nb-Ti: Nb-Ti/Ti (19/5) 370 nm multilayer '95 (0°), 50 μ V/cm - N. Rizzo et al. LTSC'96 (Yale)
- Nb-Ti: APC strand Nb-47wt.%Ti with 24vol.%Nb pins (24nm nominal diam.) - Heussner et al. (UW-ASC)
- × Nb-Ti: Aligned ribbons, B<sub>||</sub> ribbons, Cooley et al. (UW-ASC)
- - ○ - - Nb-Ti: Best Heat Treated UW Mono-Filament. (Li and Larbalestier, '87)
- - ● - - Nb-Ti: Example of Best Industrial Scale Heat Treated Composites ~1990 (compilation)
- Nb-Ti(Fe): 1.9 K, Full-scale multifilamentary billet for FNAL/LHC (OS-STG) ASC'98
- ▲ Nb-Ti: Nb-47wt.%Ti, 1.8 K, Lee, Naus and Larbalestier (UW-ASC'96) ICMC-CEC1997.
- ▲ Nb-44wt.%Ti-15wt.%Ta: at 1.8 K, monofil. optimized for high field, unpub. Lee, Naus and Larbalestier (UW-ASC'96)
- △ Nb<sub>3</sub>Sn: Internal Sn High J<sub>c</sub> design CRe1912, OI-STG, - Zhang et al. ASC'98 Paper MAA-06
- ◇ Nb<sub>3</sub>Sn: Internal Sn High J<sub>c</sub> design ORe0038, OI-STG, - Zhang et al. ASC'98 Paper MAA-06
- Nb<sub>3</sub>Sn: Internal Sn, ITER type low hysteresis loss design - (IGC - Gregory et al.) [Non-Cu J<sub>c</sub>] - Thoner et al., Erice '96.
- ▲ Nb<sub>3</sub>Sn: Bronze route int. stab. -VAC-HP, non-(Cu+Ta) J<sub>c</sub>, - Thoner et al., Erice '96.
- Nb<sub>3</sub>Sn: SMI-PIT, non-Cu J<sub>c</sub>, 10 μV/m, 36 fil., 0.8 mm dia. (42.6% Cu), - U-Twente & NHFML data provided April 29th 1999 by SMI.
- \* Nb<sub>3</sub>Sn: Tape from (Nb,Ta)<sub>6</sub>Sn<sub>5</sub>+Nb-4at.%Ta powder, [Core J<sub>c</sub>, core ~25 % of non-Cu area] Tachikawa et al. (Tokai U.), ICMC-CEC '99
- Nb<sub>3</sub>Sn: Bronze route VAC 62000 filament, non-Cu 0.1μΩ-m 1.8 K J<sub>c</sub>, - VAC/NHML data courtesy M. Thöner (Vacuumschmelze)2000'
- \* Nb<sub>3</sub>Al: Bi stabilized 2-stage JR process (Hitachi,TML-NRIM,IMR-TU), - Fukuda et al. ICMC/ICEC '96
- △ Nb<sub>3</sub>Al: 84 Fil. RHQT Nb/Al-Mg(0.6μm), Iijima et al. NRIM ASC'98 Paper MVC-04
- Nb<sub>3</sub>Al: 84 Fil. RHQT Nb/Al-Mg(0.6μm), Iijima et al. NRIM ASC'98 Paper MVC-04
- ◇ Nb<sub>3</sub>Al: DRHQ with Intermediate cold-work, core J<sub>c</sub>, - Kikuchi et al. (NRIM) ASC2000
- YBCO: /Ni/YSZ ~1 μm thick microbridge, H<sub>||</sub>c 4 K, - Foltyn et al. (LANL) '96
- YBCO: /Ni/YSZ ~1 μm thick microbridge, H<sub>||</sub>ab 75 K, - Foltyn et al. (LANL) '96
- - - YBCO: /Ni/YSZ ~1 μm thick microbridge, H<sub>||</sub>c 75 K, - Foltyn et al. (LANL) '96
- Bi-2212: 3-layer tape (0.15-0.2 mm 4.0-4.8 mm) B<sub>||</sub>tape at 4.2 K face - Kitaguchi et al. -ISS'98, 1 μV/cm
- ◇ Bi-2212: paste, B<sub>||</sub>tape, 4.2 K - Hasegawa et al. (Showa) IWS'95
- ▲ Bi-2212: stack, B<sub>||</sub>tape, 4.2 K - Hasegawa et al. (Showa) IWS'95
- - ▲ - - Bi-2212: 19 filament tape B<sub>||</sub>tape face - Okada et al (Hitachi) '95
- Bi-2212: Round multifilament strand - 4.2 K - (IGC) Motowidlo et al. ISTEC/MRS '95
- Bi-2223: multi, B<sub>||</sub>tape, 4.2 K - Hasegawa et al. (Showa) IWS'95
- Bi 2223: Rolled 85 Fil., Tape, B<sub>||</sub>, - (AmSC) UW'6/96
- ▲ Bi 2223: Rolled 85 Fil. Tape, B<sub>||</sub>, - (AmSC) , UW'6/96
- PbSnMo<sub>6</sub>S<sub>8</sub> (Chevrel Phase): Wire with 20%SC in 14 turn coil, - (Univ. Geneva/HFML&RIM - NL/U-Rennes, 97



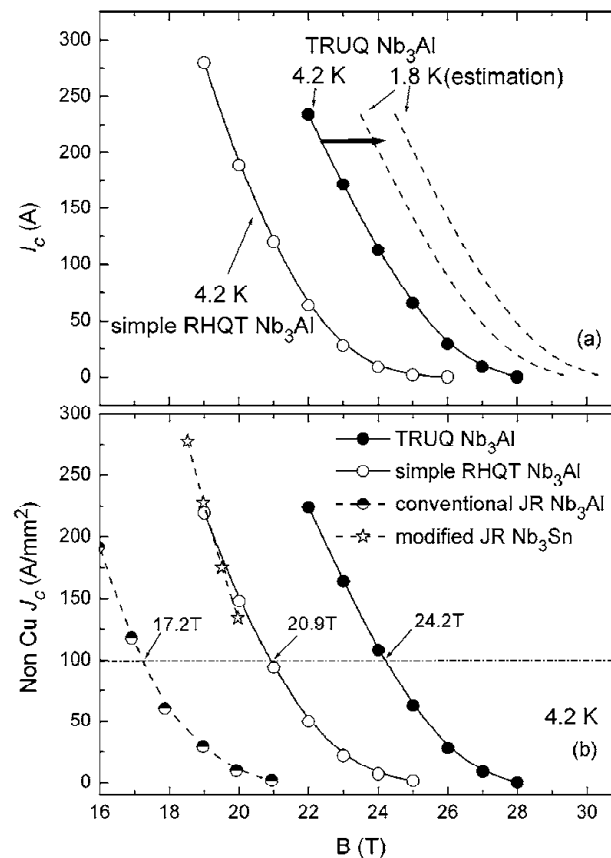


# TRUQ



**Figure 2.** Illustration of TRUQ: (a) the propagation of the transformation interface from the left to the right in a Nb/Nb(Al) composite quickly pushed into 1000 °C region in a gold-mirror furnace, (b) the enthalpy release during the transformation from bcc to A15 and (c) the temperature profile for the whole heat treatment process.

From Takeuchi et al. Sc. Sci. Tech. Vol.13, 2000

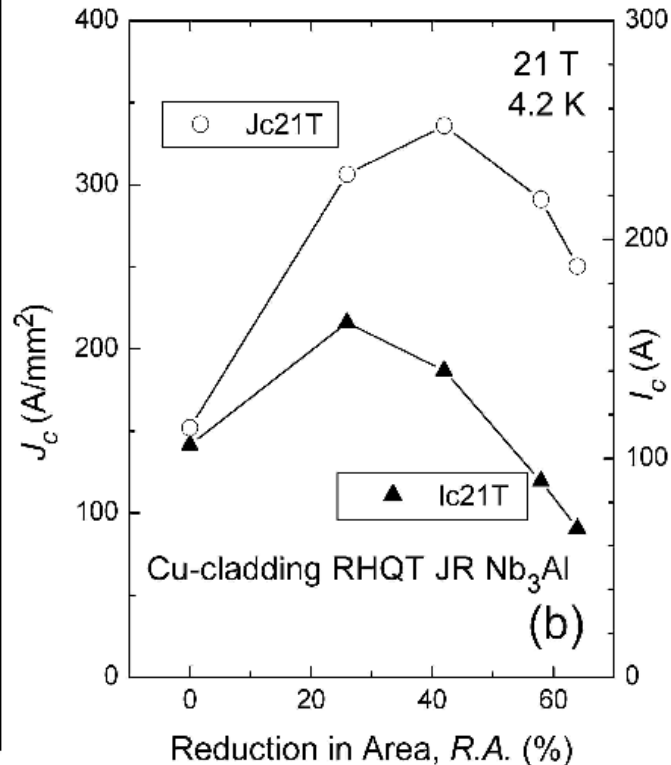
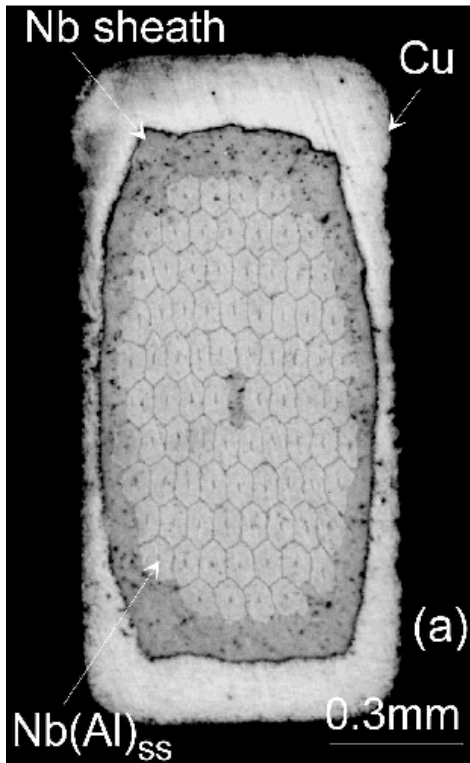


**Figure 3.** (a) and (b) non-Cu versus curves of TRUQ-processed  $\text{Nb}_3\text{Al}$  tape conductor (3.5 mm in width and 0.3 mm in thickness), in comparison with those of conventional, low-temperature-processed, JR  $\text{Nb}_3\text{Al}$  [17] and simple RHQT, JR  $\text{Nb}_3\text{Al}$  (1.25 mm in diameter) [4] conductors, and a modified JR  $\text{Nb}_3\text{Sn}$  conductor [18]. An estimation of (1.8 K) of TRUQ  $\text{Nb}_3\text{Al}$  is made by shifting the (4.2 K) data toward the higher field by 1.5–2.5 T.





# Cladding of RHQT - NRIM



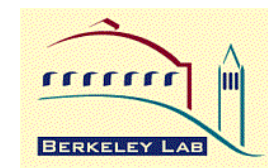
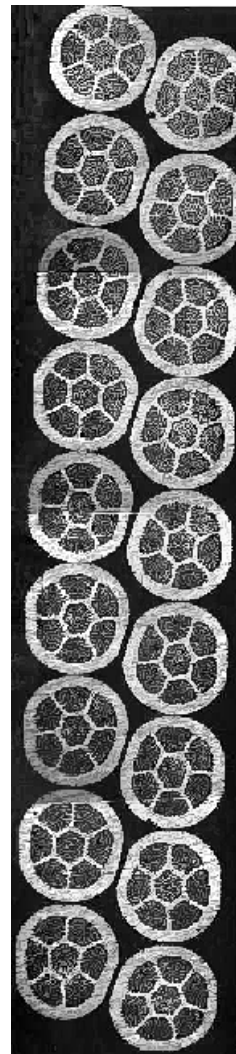
External stabilization for RHQT JR Nb<sub>3</sub>Al by mechanical cladding method: (a) transversely overall cross-sectional image, (b)  $J_c$  and  $I_c$  against R.A. at Cu-cladding.

From: Takeuchi et al. ASC 2000 paper 5ML02



# ***Bi-2212 round wire continues to show promise for accelerator magnets***

- $J_c(12\text{ T}, 4.2\text{ K}, \text{non-Ag}) > 1500\text{ A/mm}^2$  in new material (ASC2000 paper 2MC03)
- Long lengths(  $> 250\text{ m}$ ) are being produced; scale-up to  $>1000\text{ m}$  unit lengths is in progress.
- $J_c$  vs strain for Rutherford cables looks promising(ASC 2000 paper 4MG06)
- React and wind coils are being made (ASC 2000 paper 3LE06)
- cost is still a major issue



**Ron Scanlan  
ASC2000**

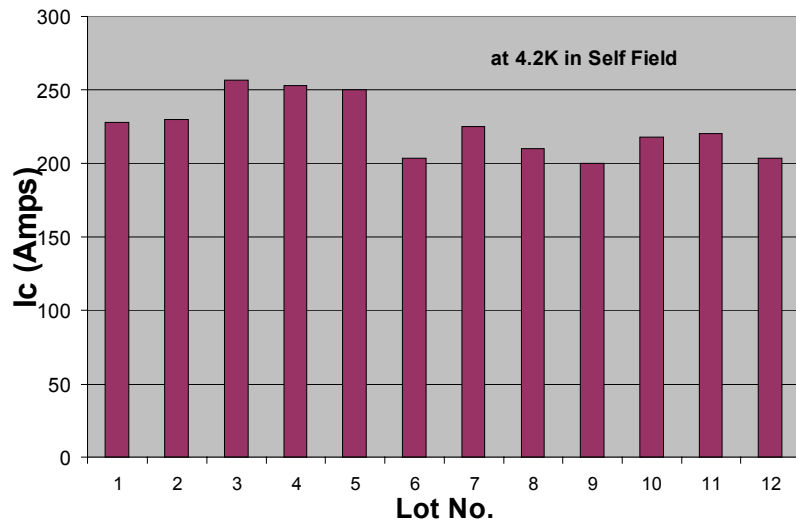
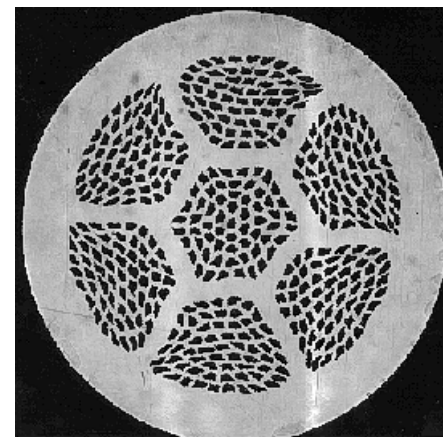
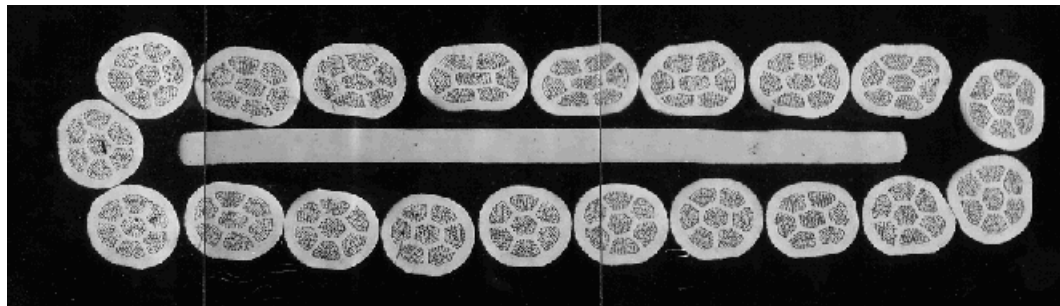




# Bi-2212 IGC-AS

BSCCO-2212 0.81mm wire

427 filaments, 15 $\mu$ m filament diameter



*L. Motowidlo, R. Sokolowski IGC-AS*

*T. Hasegawa, Showa Electric*

*R. Scanlan, LBNL*

80 m of cable fabricated

$I_c$  in self-field 3000 A

From Arup K. Ghosh, BNL Accelerator  
Magnet Divn: VLHC-FNAL Magnet  
Technologies Workshop





# BSSCO-2223 Multifilament Tape

Conductors for BNL HTS coils

		Vendor	Length [m]	Width [mm]	Thickness [mm]	$I_c$ (77K,SF) [A]	$J_e$ [A/mm]	Axial stress [Mpa]	Matrix
1998	IGC	6x100	3.55	0.22	25	32			Ag
1999	NST	210	3.02	0.238	27	38	150		Ag-alloy
1999	NST	590	3.02	0.238	31	43	150		Ag-alloy
1999	VAC	155	3.78	0.22	53	64	>90		Ag-Mg
1999	VAC	155	3.82	0.23	58	66	>90		Ag-Mg
1999	VAC	155	3.86	0.23	58	65	>90		Ag-Mg
2000	ASC	210	3.04	0.171	68	131	75		Ag-alloy
2000	ASC	210	3.04	0.175	71	134	75		Ag-alloy
2000	ASC	210	3.13	0.175	81	148	75		Ag-alloy
2000	ASC	210	2.93	0.163	70	147	75		Ag-alloy

Cost \$25/m

From Arup K. Ghosh, BNL Accelerator Magnet Divn:  
VLHC-FNAL Magnet Technologies Workshop

**BROOKHAVEN**  
NATIONAL LABORATORY





# ***What does the future hold for HTS***

- YBCO needs a lot of development before it can be a realistic conductor for magnets.
  - Conductor of choice for magnets operating at temperatures  $> 20$  K
- BSCCO-2223 has slowly but steadily improved. Km lengths of reasonable  $J_c$  are feasible. More uniform conductor now available with improved manufacturing techniques
- BSCCO-2212 is potentially a better choice than 2223 at 4.2 K.
  - Probably will be less costly than 2223.
  - Can be fabricated as a tape or round wire suitable for Rutherford cables
  - Potential  $J_c$  at 12 T exceeding that of  $Nb_3Sn$

From Arup K. Ghosh, BNL Accelerator Magnet Divn:  
VLHC-FNAL Magnet Technologies Workshop

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## ***FY 01 and beyond ....***

- Continue programs at IGC and OST
- New Conductor Initiatives
  - Powder in tube RFP (anticipate 3-4 responses)
  - Nb<sub>3</sub>Al Precursor Fabrication RFP (anticipate 3-4 responses)
  - Special processing facilities
- Additional support for heat treatment, characterization, and  $I_c$  testing work
- Scale-up key manufacturing steps to establish large scale processing costs
- Develop realistic cost data to include in VLHC design studies



**Ron Scanlan ASC2000**





# ***New Materials Program--Summary***

- New Materials Program is underway, with broad community support and participation
- Two contracts are in place (IGC-AS and OI-ST)
- Nb<sub>3</sub>Sn manufacturers are using this as an opportunity to rebuild their development teams
- I am optimistic that we can meet the performance and cost goals for Nb<sub>3</sub>Sn
- Nb<sub>3</sub>Al and Bi-2212 show promise as potential high field dipole conductors



**Ron Scanlan ASC2000**





# ***VLHC Conductor 2000 Summary***

- Conductor Development Program Started - *at last the major suppliers get direct HEP focused research money.*
- Internal Sn in transition to high  $J_c$  and lower cost. *What should our  $J_c$  vs \$\$\$ balance be at this point?*
- Nb<sub>3</sub>Al: the most progress in 2000 but still expensive and developments are for short lengths. *How important is strain intolerance - with magnet design advances?*
- HTS slow but steady progress. *How long would you like to wait?*

